



#### **CERTIFICATE OF PLAN APPROVAL**

This is not a Building Permit. It is a record of our review of documents submitted with your application for a Building Permit.

26 October 2020

Ms. Brenda Kinser O'Neil Tents 895 W. Walnut Street Canal Winchester, OH 43110 (614) 837-6352 <u>bjk@oneiltents.com</u>

Re:	Tucci's Patio Winter Tent			
Address:	35 N. High Street (43017)			
Application No.:	TSTR-20-01723(1)			

Dear Ms. Kinser:

The construction documents dated 25 September 2020 have been reviewed for compliance with the provisions of the 2017 Ohio Building Code (August 2018 Edition). The review was based upon the following criteria:

Primary Use Group: Area/Occupant Load:	A-2 1,849 SF / Chairs @ Tables shown = 62 Seats* *Reference all current Governor of Ohio's "Responsible RestartOhio" regulations and guidance for social distancing requirements
Construction Type:	IIB
Special Stipulations:	<ol> <li>Set up 1 November 2020; Take down by 29 April 2021(&lt;180 days) or until the end of the Executive Order, whichever is first.</li> <li>This approval is for the 43'x43' main tent only.</li> <li>No cooking allowed.</li> </ol>
Project Description:	Temporary structure to create additional eating area for Tucci's restaurant as allowed by City of Dublin "Executive Order for Portable Structures and Temporary Uses" related to COVID-19 State of Emergency (March 17, 2020). Tent consists of a clear span 43'-0"X43'-0" enclosed, heated structure anchored to new concrete piers with two illuminated exit signs/egress lights w battery back-up and 2 fire extinguishers.
Previous Occ Cert:	TSTR-20-00999 (summer tent): 12-200470 (building)

The construction documents were prepared by Robert V. Nangia, Ohio registered engineer #E-73309 and Jeffery R. Bolchalk, Ohio registered engineer #E-70796 to comply with the

11/03/20

City of Dublin

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requirements of the OBC Section 107.4.3 and have been reviewed, therefore, in accord with that Section.

**OBC 107.5.1 Approval of construction documents.** . . . When the construction documents have been determined to conform to the applicable provisions of the rules of the Board, the building official shall endorse or stamp such plans as approved and issue the certificate of plan approval in accordance with section 105.5.

#### Item 1 THE CONSTRUCTION DOCUMENTS ARE APPROVED

Item 2 The qualification of Geotechnical Consultants, Inc. as the Special Inspection company for all foundation and structural work has been reviewed and accepted by the building official.

**1704.2.4 Report requirement.** *Special inspectors* shall keep records of inspections. The *special inspectors* shall submit reports of special inspections and tests to the building official and to the registered design professional in responsible charge. Reports shall indicate that work inspected or tested was or was not completed in conformance to approved construction documents. Discrepancies shall be brought to the immediate attention of the contractor for correction. If they are not corrected, the discrepancies shall be brought to the attention of the building official and to the registered design professional in responsible charge prior to the completion of that phase of the work. A final report documenting required special inspections and tests, and correction of any discrepancies noted in the inspections or tests, shall be submitted at a point in time agreed upon prior to the start of work by the owner or the owner's representative to the building official prior to the *issuance of a certificate of occupancy*.

## This APPROVAL is for the issuance of a general building permit only. Separate permits and fees for plumbing, mechanical, sprinkler, electric and low-voltage must be obtained from the Dublin Building Standards Division prior to the start of any work in these generally subcontracted areas.

The following items are required for code compliance, but are not necessarily covered in detail in the construction documents. This list is a reminder to the design professional and contractors of issues, which are to be satisfactorily dealt with in the field:

- **Item A** Review and Approval of Plumbing Drawings and inspection of Plumbing installations are performed by the Franklin County Board of Health
- Item B OBC 106.3 Amended construction documents. If substantive changes to the building are contemplated after first document submission, or during construction, those changes must be submitted to the building official for review and approval prior to those changes being executed. The building official may waive this requirement in the instance of an emergency repair, or similar instance.



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- **OBC 107.5.2 Posting.** The certificate of plan approval shall be posted in a Item C conspicuous location on the site. The owner and the contractor shall preserve and keep the certificate posted until the final inspections are complete.
- Item D OBC 107.7 Approved construction document sets. One set of construction documents shall be kept by the building official. The other set(s) shall be returned to the applicant, kept at the work site along with manufacturers' installation instructions and product information, and shall be available for use by the inspector.
- Item E **OBC 108.1 General.** . . . Construction or work for which an approval is required shall be subject to inspection by the building official. It shall be the duty of the owner or the owner's duly authorized representative to notify the building department when work is ready for inspection. Access to and means for inspection of such work shall be provided for any inspections that are required by this code.

It shall be the duty of the owner or the owner's authorized representative to cause the work to remain accessible and exposed for inspection purposes . . . until the work has been inspected to verify compliance with the approved construction documents. . .

This includes firestopping and draftstopping, mechanical work; piping, ducts and systems, structural members and connections, and electrical work (Chapter 27 OBC). All systems and elements covered by code are to be inspected and approved before being covered.

Subsequent work is allowed to proceed only to the point of the next required inspection.

- **OBC 804.3 Testing and Identification** Interior floor finish and floor covering Item F materials shall be tested by an approved agency in accordance with NFPA 253 and identified by a hang tag or other suitable method so as to identify the manufacturer or supplier and style, and shall indicate the interior floor finish or floor covering classification according to Section 804.2. Carpet-type floor coverings shall be tested as proposed for use, including underlayment. Test reports confirming the information provided in the manufacturer's product identification shall be furnished to the building official upon request.
- OBC 1101.2 Design. Buildings and facilities shall be designed and constructed Item G to be accessible in accordance with this code and ICC 117.1 as amended in Section 1112 of this chapter.
- All electrical will comply with the requirements of Article 27 OBC and the National Item H Electrical Code, NFPA 70, OBC approved.

Reviewed and Signed,

#### J.E. Rusanowsky

Janet E. Rusanowsky, Architect **Commercial Plans Examiner** (614) 410 4612 irusanowsky@dublin.oh.us

Brad Fagrell Brad Fagrell, P.E.

Director of Building Standards/CBO



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Owner or Owner's Representative

Date

Print Name and Title as Signed



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#### EXECUTIVE ORDER

#### TEMPORARY OUTDOOR PATIO EXPANSION

Pursuant to Chapter 36 of the Dublin Codified Ordinances and the City Manager's Declaration of a State of Emergency issued on March 17, 2020, the enforcement of certain provisions of Chapter 153 regarding the City's Outdoor Dining and Seating regulations are temporarily amended as follows:

- 1. A business may temporarily expand their outdoor dining and eating area outside of the currently designated/approved location to allow for increased social distancing related to COVID-19. This will be permitted with the following stipulations:
  - a. The expansion will be permitted in conjunction with an existing and permitted restaurant use;
  - b. A Certificate of Zoning Plan Approval will be required at no cost;
  - c. Relief from specific zoning site requirements, design details, and parking requirements will be applied on a case-by-case basis.
  - d. Outdoor speakers and music will not be permitted in the expanded areas.
  - e. Outdoor dining and seating area materials should complement the existing materials.
  - f. Expanded areas will be located to be sensitive to and take into consideration surrounding properties, including residential areas.
  - g. Alcohol may only be served in the expanded area when permitted by the Ohio Division of Liquor Control.
  - h. Staff will review the request for the expansion in conjunction with the direction and guidance of FCPH.
- 2. A Certificate of Zoning Plan Approval shall be required in order to permit Outdoor Dining and Seating expansion. The following information will be required to be submitted with the CZPA form at no charge:
  - Detailed, dimensioned site plan showing the location on the site with adherence to ensuring safe access and be served by adequate parking;
  - Sensitively located and to show adherence to the standards of the community and minimizing impact on nearby residential uses to the maximum extent possible;
  - Design specifications associated with the proposed outdoor dining and seating expansion shall be provided: chairs and tables, umbrellas, etc.
  - Detailed narrative noting the specific use proposed and the scope of the intended use, particularly highlighting the required need as a result of COVID-19;
  - Signed acknowledgment that the time period of validity is limited to the City's designation of a State of Emergency, or any other time limitation otherwise mandated by the City Manager.

The intent of this Order is to support and promote increased social distancing and support local businesses during this difficult economic time. These temporary amendments will immediately cease upon termination of the State of Emergency or as otherwise mandated by the City Manager and the expanded outdoor dining and seating will be required to be removed and site restored.



#### EXECUTIVE ORDER

#### PORTABLE STRUCTURES AND TEMPORARY USES

Pursuant to Chapter 36 of the Dublin Codified Ordinances and the City Manager's Declaration of a State of Emergency issued on March 17, 2020, the enforcement of certain provisions of Chapter 153 regarding the City's Portable Structures and Temporary Uses are temporarily amended as below:

- Section 153.097(B)(3) Portable Nonresidential Structures. A business may temporarily erect a building(s) or similar structure(s) designed for occupation which is not placed on a permanent foundation to allow for testing, waiting or staging related to COVID-19. The definition shall include construction trailers, portable classrooms, tents, trailers and other similar structures.
- Section 153.097(C) Permit process. A Certificate of Zoning Plan Approval shall be required to permit these designated portable structures and temporary uses. The following information will be required to be submitted with the CZPA form at no charge:
  - Detailed, dimensioned site plan showing location on the site with consideration of the required setbacks and ensuring safe access and be served by adequate parking;
  - Sensitively located to show adherence to the standards of the community and minimizing impact on nearby residential uses to the maximum extent possible;
  - Detailed and dimensioned elevations or design specifications of the proposed temporary structure;
  - Detailed in a narrative noting the specific use proposed and the scope of the intended use, particularly highlighting the required need as a result of COVID-19;
  - Signed acknowledgment that the time period of validity is limited to the City's designation of a State of Emergency, or any other time limitation otherwise mandated by the City Manager.

The intent of this Order is to support and promote healthy practices during this difficult economic time. These temporary amendments will immediately cease upon termination of the State of Emergency or as otherwise mandated by the City Manager and the portable structures and temporary uses will be required to be removed and the site restored.

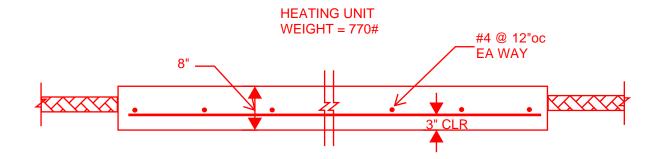
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	inc.com	

 Project Name: Tucci's			
 Project Number: 2014.87	Subject: Heating Unit Sla	ab	I C
 Date: 11/05/2020	Author: CMM	Page: 1	schæfer





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### **Gable Style Single-level Structure**

#### 13m x 13m - 3.2m Eave

### Structural evaluation of the gable style structure in accordance with IBC 2015, and ASCE7-10

Designed for wind velocity 115 mph basic wind speed, 3-second gust, Exposure B with factors applied per ASCE37-02 for nominal wind design pressures

Risk Category = 'll' Ground snow = 20 psf Enclosed Structure



#### ROBERT V. NANGIA P.E. 7423 HOLLOW RIDGE DR. HOUSTON, TX 77095

The professional engineer seal on this cover page refers to the calculation sheets contained within this document and to any Appendix or Table sheets that support this document. Any other drawings and documents may require a separate seal for coverage not provided here. Certification of this document only shows that the Professional Engineer of that particular state is in agreement with the report's contents. It does not, however, imply that the structure is generally suitable for use within that state, or that every installation is covered by this report. The information and illustrations contained within this document remain the sole property of HTS tentIQ and are to be treated as confidential. The professional engineer's seal, affixed on this document, signifies a responsibility for the structural adequacy of the design of the structure in the completed project. The content contained within this document does not encompass means, methods and safety of erection. All data, designs, technical representations, engineering calculations and illustrations whether written or implied may not be reproduced in whole or in part nor distributed, used in manufacturing, design or display without the express written consent of HTS tentIQ. Retention of this document shall constitute acceptance of these terms and conditions.



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### **Revision Log**

RevRev. DateDescription031 Aug 20- Original Issue



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#### 1. Summary and Recommendations

- This document, based on technical background information as provided by HTS tentIQ, covers the structural evaluation of the aluminum frame style structure in accordance with U.S. Building Code requirements. The specifications outlined in the Structural Engineering Institute / American Society of Civil Engineers (SEI/ASCE 7) "Minimum Design Loads for Buildings and Other Structures" were followed in determining the integrity of the structure. This document is intended to serve as a basis for the acceptability of this temporary, stand-alone, enclosed structure under standard design wind loads at varying levels of exposure (terrain and wind velocities).
- Lightweight Design Inc. compiled this document based on the existing frame tent system with reference to the applicable building codes in the U.S. This report includes the load cases and combinations used in the analysis and gives an indication as to the wind exposure for which the structure is suitable. Certification of this document only shows that the Professional Engineer of that particular state is in agreement with the report's contents. It does not, however, imply that the structure is generally suitable for use within that state, or that every installation is covered by this report.
- Computer-aided structural frame analysis were involved in the course of the investigation. Different load combinations were considered to identify the critical aspects of the design. Member and detail checks were established to derive the conclusions for the entire report.

As such, we have arrived at the following conclusions and recommendations:

#### 1.1 Wind Speed Rating

- Wind Speed
- 115 mph, 3-second gust
- Exposure Category B
  - Construction Period Period = "More than 5 years"
- Velocity Pressure  $q_h = 20.16 \text{ psf}$  at mean roof height, h = 14.19 ft

#### Exposure Categories (IBC)

- **1609.4.3 Exposure categories.** An exposure category shall be determined in accordance with the following:
  - **Exposure B.** Exposure B shall apply where the ground surface roughness condition, as defined by Surface Roughness B, prevails in the upwind direction for a distance of at least 2,600 feet (792 m) or 20 times the height of the building, whichever is greater.
  - **Exception:** For buildings whose mean roof height is less than or equal to 30 feet (9144 mm), the upwind distance is permitted to be reduced to 1,500 feet (457 m).
  - Exposure C. Exposure C shall apply for all cases where Exposures B or D do not apply.
  - **Exposure D.** Exposure D shall apply where the ground surface roughness, as defined by Surface Roughness D, prevails in the upwind direction for a distance of at least 5,000 feet (1524 m) or 20 times the height of the building, whichever is greater. Exposure D shall extend inland from the shoreline for a distance of 600 feet (183 m) or 20 times the height of the building, whichever is greater.



#### Surface Roughness Categories (IBC)

**1609.4.2 Surface roughness categories.** Aground surface roughness within each 45-degree (0.79 rad) sector shall be determined for a distance upwind of the site as defined in Section 1609.4.3 from the categories defined below, for the purpose of assigning an exposure category as defined in Section 1609.4.3.

**Surface Roughness B.** Urban and suburban areas, wooded areas or other terrain with numerous closely spaced obstructions having the size of single-family dwellings or larger.

- Surface Roughness C. Open terrain with scattered obstructions having heights generally less than 30 feet (9144 mm). This category includes flat open country, grasslands, and all water surfaces in hurricane-prone regions.
- **Surface Roughness D.** Flat, unobstructed areas and water surfaces outside hurricane-prone regions. This category includes smooth mud flats, salt flats and unbroken ice.

#### 1.2 Hanging Dead Loads

The electrical and mechanical fixtures (lighting, HVAC, suspended items, etc.) totaling 500 lbs per frame and suspended symmetrically on the structure are accounted for. These hanging loads have been assumed to be 125 lbf at the center of each rafter and 250 lbf at the ridge of each rafter for this analysis.

#### 1.3 Live Loads (Snow, Floor, Roof)

Ground snow loading for the area is 20 psf.

Live loads loads produced by the use and occupancy of the building are found on Table 1607.1. n the case of this structure, there are no additional live loads.

Based on performance and function of this building style, only short duration of the roof live load is expected on the fabric roof of the structure. If repairs are needed, usually one worker with a light equipment would suffice. Roof Live Load is not considered for this evaluation.

#### 1.4 Base Reactions

- The maximum reactions at the foundations/supports due to service and combined loads reactions and exposure category are given in the Appendix C
- NOTE: Foundations, by others, are required to support column loads. A foundations engineer must verify ground conditions on a site-by-site basis and provide appropriate bearing plate sizes to accommodate column loads:

#### 1.5 Installation Requirements

- It is understood that the responsibility of proper installation according to the plans rests upon the installation contractor. This includes, but is not limited to, ensuring the following:
  - that the cables are always held taut,
  - that the fabric is stretched tight enough to prevent the development of pockets and to maintain the prescribed roof gradient,
  - that purlins are installed securely against rafters to resist calculated loads,
  - that base plates are secured to their foundations using anchors. The manufacturer
    provides a base plate and anchoring plan for the structure as a base starting point for
    average soil conditions. It is the installers responsibility to ensure that the anchorage
    provided will resist the reaction loads as indicated in the tables found in this
    document.



#### 2a. Determination of Loads

#### Dead Load :

The structure dead loads consist of the self weight of the structure's components with addition of uniform distributed loads for fabric roofing, side wall materials, and minor components. Various calculated weights are shown below for reference and use in the static computer model analysis.

The structure is designed to support the loads shown in this calculations. It may, or may not, be capable of supporting additional collateral loads. The owner of the structure shall not hand, or otherwise affix, additional loads to this structure without a review by an engineer qualified to make said review. Additionally, prior to adding load to this structure, the owner shall get a written confirmation by the qualified engineer as to the magnitude and location of the load, or loads, being applied.

The electrical and mechanical fixtures (lighting, HVAC, suspended items, etc.) totaling 500 lbs per frame and suspended symmetrically on the structure are accounted for. These hanging loads have been assumed to be 250 lbf at the peak of the structure and 125 midway up each rafter for this analysis.

Load hanging at peak :	$P_{peak} = 250 \cdot lbf$
Rafter load hanging midway between peak and eave :	$P_{rafter} = 125 \cdot lbf$

#### Live Load :

Live loads loads produced by the use and occupancy of the building are found on Table 1607.1. In the case of this structure, there are no additional live loads.

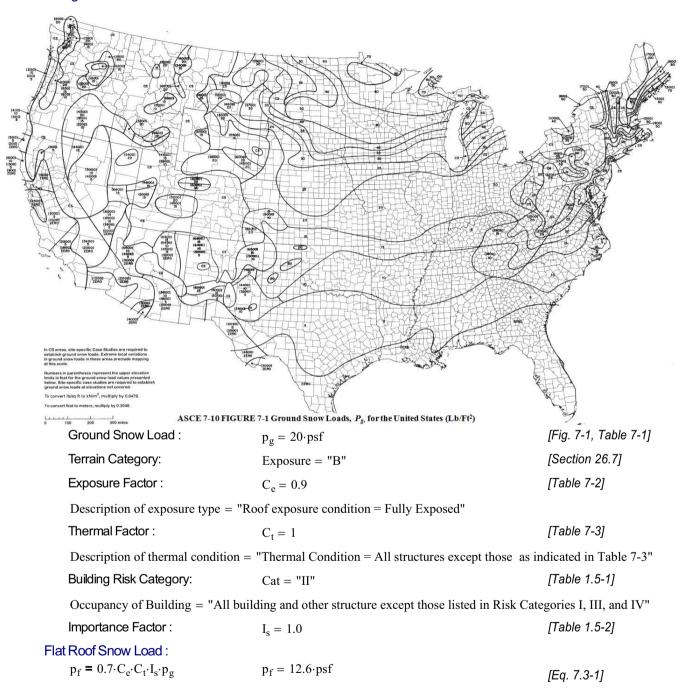
#### **Roof Live Load :**

Live loads loads produced by the use and occupancy of the building are found on Table 1607.1. In the case of this structure, the mezzanine can be described as having a uniformly distributed load for walkways and elevated platforms. The minimum floor live load used in this evaluation is 0 psf.



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#### 02b. Determination of Loads-Snow Loads Design Parameters





#### Minimum Snow Load for Low-Slope Roofs :

Per ASCE 7-10 Section 7.3.4, minimum roof snow load, p<sub>m</sub>, shall only apply to monoslope, hip and gable roofs with slopes less than 15°, and to curved roofs where the vertical angle from the eaves to the crown is less than 10°. This minimum roof snow load is a separate uniform load case. It need not be used in determining or in combination with drift, sliding, unbalanced, or partial loads.

Check for Minimum Snow Load = "minimum values for low-slope roof need not to be considered "

#### Sloped Roof Snow Load

Roof Slope Factor :	$C_{s} = 0.80$	[Figure 7-2a]
Sloped Roof Load :	$\mathbf{p}_{s} = \mathbf{C}_{s} \cdot \mathbf{p}_{f}$	[Eq. 7.4-1]
	$p_s = 10.11 \cdot psf$	

#### Rain-on-Snow Surcharge Load:

Per ASCE 7-10 Section 7.10, for locations where p<sub>a</sub> is 20 psf or less, but not zero, all roofs with slopes (in

degrees) less than W/50 with W in feet shall include a 5 psf rain-on-snow surcharge load. This additional load applies only to the sloped roof (balanced) load case and need not be used in combination with drift, sliding, unbalanced, minimum, or partial loads.

Rain-on-Snow Surcharge Load = "surchage load need not be applied"

Design Balanced Snow Load :

 $p_s = 10.11 \cdot psf \qquad S_0 \textbf{=} p_s \cdot L_{bay}$ 

 $S_0 = 37.05 \cdot pli$ 

#### Design Unbalanced Snow Load Design Check:

Per ASCE 7-10 Section 7.6.1, for hip and gable roofs with a slope exceeding 7 on 12 ( $30.2^{\circ}$ ) or with a slope less than 2.38° ( $\frac{1}{2}$  on 12) unbalanced snow loads are not required to be applied.

 $\theta_{\rm roof} = 17.86 \cdot \deg$ 

[Section 7.6.1]

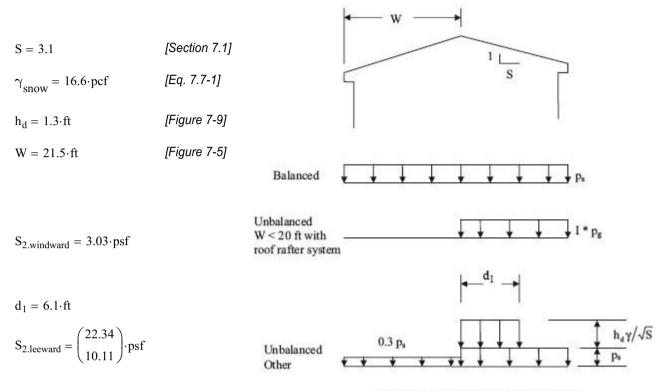
[Section 7.10]

Check unbalanced load requirement = "all criteria met; must consider unbalanced loads"



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#### Design Unbalanced Snow Load :

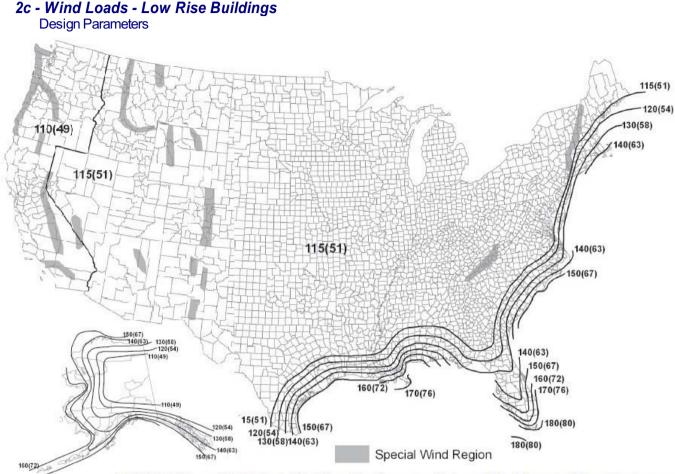


ASCE 7-10 FIGURE 7-10 Balanced and Unbalanced Snow Loads for Hip and Gable Roofs.



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\*ASCE 7-10 Figure 26.5-1A Basic Wind Speed for Occupancy Category II Buildings and Other Structures.

**Risk Category:** [Table 1.5-1] Cat = "II"Occupancy of Building = "All building and other structure except those listed in Risk Categories I, III, and IV" Basic Wind Speed: [Section 26.5.1]  $V = 115 \cdot mph$ Wind Directionality Factor: [Table 26.6-1]  $K_{d} = 0.85$ Exposure Category: [Section 26.7] Exposure = "B" Topographic Factor: [Section 26.8.2]  $K_{zt} = 1$ **Gust Effect Factor:** [Section 26.9.1] G = 0.85Enclosure Classification: [Section 26.12] Enclosure = "Enclosed"

#### Wind Velocity Reduction for Temporary Structure per ASCE37-02

Reduction Factor: Construction Period: Effective Wind Speed:	$R_n = 1$ Period = "More than 5 years" $V_r = 115 \cdot mph$	[ASCE 37-02 Section 6.2.1]	City of Dublin
02c Determination of Loads-Wind (Low-	1 of 4		Approved for Construction
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#### Envelope Procedure for Low Rise Buildings - ASCE 7-10 Chapter 28

Per ASCE 7-10 Section 26.2, buildings with mean roof height *h* less than or equal to 60 ft, and with mean roof height *h* dose not exceed least horizontal dimension are considered as low-rise building.

Check Low Rise Criteria = "both low-rise conditions are satisfied"

Per ASCE 7-10 Section 28.1.4, no reduction to the velocity pressure is taken due to apparent shielding.

Velocity Pressure :

$q_z = 0.00256 \cdot K_z \cdot K_{zt} \cdot K_d \cdot V_r^2$	velocity pressure evaluated at peak height	[Section 28.3.2;
$q_h = 0.00256 \cdot K_h \cdot K_{zt} \cdot K_d \cdot V_r^2$	velocity pressure evaluated at mean roof height	Equation 28.3-1]
where : for $15 {\rm ft} \le z \le z_g$	for $z \le 15$ ft	
$\frac{2}{\alpha}$	$\frac{2}{\alpha}$	[Table 28.3-1]
$K_z = 2.01 \cdot \left(\frac{z}{z_g}\right)^{cc}$	$K_z = 2.01 \cdot \left(\frac{15ft}{z_g}\right)^{ct}$	

\*Note: z shall not be taken less than 30 feet in exposure B.

$z_g = 1200 \cdot ft$		[Table 26.9.1]
K <sub>z</sub> = 0.7	velocity pressure exposure coefficient evaluated at peak height ( $z = 17.66  ft$ )	
$K_h = 0.7$	velocity pressure exposure coefficient evaluated at mean roof height ( $h = 14.19  ft$ )	
$q_z = 20.16 \cdot psf$	velocity pressure evaluated at building height, z	
$q_h = 20.16 \cdot psf$	velocity pressure evaluated at mean roof height, h	



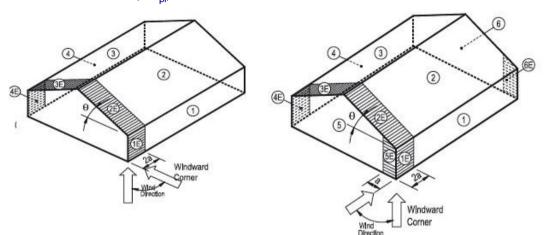
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[Equation 28.4-1]

#### **Design Wind Pressure**

 $p = q_h \cdot \left[ \left( GC_{pf} \right) - \left( GC_{pi} \right) \right]$ 

External Pressure Coefficients (GC<sub>nf</sub>)



Load Case A

Load Case B

ASCE 7-10 FIGURE 28.4-1 External Pressure Coefficients (GCpf)

Transverse Direction	(Load Case A)
----------------------	---------------

$GC_{mfA} =$	"1"	"2"	"3"	"4"	"1E"	"2E"	"3E"	"4E"	$a = 4.3 \cdot ft$
$GC_{pf,A} =$	0.51	-0.69	-0.46	-0.41	0.77	-1.07	-0.67	-0.61	
									$2 \cdot a = 8.60 \cdot ft$

(interpolated to the roof slope at:  $\theta_{roof} = 17.86 \text{ deg}$ )

Longitudinal Direction (Load Case B)

$GC_{r} =$	"1"	"2"	"3"	"4"	"5"	"6"	"1E"	"2E"	"3E"	"4E"	"5E"	"6E"
$GC_{pf.B} =$	-0.45	-0.69	-0.37	-0.45	0.4	-0.29	-0.48	-1.07	-0.53	-0.48	0.61	-0.43

#### Application of Pressures on Building Surfaces 2 and 3

Per note 8 in ASCE 7-10 Fig. 28.4-1, the roof pressure coefficient (GCpf), when negative in Zone 2 and 2E, shall be applied in Zone 2/2E for a distance from the edge of the roof equal to 0.5\*horizontal dimension of the building parallel to the direction of the MWFRS being designed or 2.5\* the eave height at the windward wall, whichever is less; the remainder of Zone 2/2E extending to the ridge line shall use the pressure coefficient (GCpf) for Zone 3/3E.

Zone 2/2E Distance<sub>CaseA</sub> =  $21.5 \cdot ft$ 

Zone 2/2E Distance<sub>CaseB</sub> =  $22 \cdot \text{ft}$ 

#### Internal Pressure Coefficients (GC<sub>pi</sub>)

GC: =	"Overpressure"	0.18
oopi	"Underpressure"	-0.18

[Table 26.11-1]



#### Wind at Transverse Direction (Load Case A)

	"1"	"2"	"3"	"4"	"1E"	"2E"	"3E"	"4E"	
$p_A =$	6.68	-17.54	-12.99	-11.90	11.95	-25.20	-17.08	-15.93	∙psf
	13.94	-10.28	-5.73	-4.64	19.21	-17.94	-9.82	-8.67	

\*top line = overpressure, bottom line = underpressure

#### Wind at Longitudinal Direction (Load Case B)

	"1"	"2"	"3"	"4"	"5"	"6"	"1E"	"2E"	"3E"	"4E"	"5E"	"6E"	
$p_B =$	-12.7	-17.54	-11.09	-12.7	4.44	-9.48	-13.31	-25.2	-14.31	-13.31	8.67	-12.3	∙psf
	-5.44	-10.28	-3.83	-5.44	11.69	-2.22	-6.05	-17.94	-7.06	-6.05	15.93	-5.04	

\*top line = overpressure, bottom line = underpressure

#### Design Wind Pressure on Gable

	"5"	"6"	"5E"	"6E"	
$p_g =$	4.44	-9.48	8.67	-12.3	∙psf
	11.69	-2.22	15.93	-5.04	

#### Minimum Design Wind Loads

Per ASCE 7-10 Section 28.4.4, the wind load to be used in the design of the MWFRS for an enclosed or partially enclosed building shall not be less than 16 psf multiplied by the wall area of the building and 8 psf multiplied by the roof area of the building projected onto a vertical plane normal to the assumed wind direction.



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#### 3. LRFD Load Combinations :

#### ASCE 7 -10 Section 2.2 : SYMBOLS AND NOTATION

- D = dead load
- Di = weight of ice
- E = earthquake load
- F = load due to fluids with well-defined pressures and maximum heights
- Fa = flood load
- H = load due to lateral earth pressure, ground water pressure, or pressure of bulk materials
- L = live load
- Lr = roof live load
- R = rain load
- S = snow load
- T = self-straining force
- W = wind load

Wi = wind-on-ice determined in accordance with Chapter 10

#### ASCE Section 2.3 : COMBINING FACTORED LOADS USING STRENGTH DESIGN

- Section 2.3.2 : Basic Combinations. Structures, components, and foundations shall be designed so that their design strength equals or exceeds the effects of the factored loads in the following combinations:
  - 1.1.4D
  - 2. 1.2D + 1.6L + 0.5(Lr or Sor R) 3. 1.2D + 1.6(Lr or S or R) + (L or 0.5W) 4. 1.2D + 1.0W + L + 0.5(Lr or S or R) 5. 1.2D + 1.0E + L + 0.2S 6. 0.9D + 1.0W 7. 0.9D + 1.0E

#### NOTE:

1. As it is unlikely that this structure will experience service loads F and H, they are not shown in the combinations here for clarity.

#### Exceptions :

- The load factor on L in combinations 3, 4, and 5 is permitted to equal 0.5 for all occupancies in which L<sub>o</sub> in Table 4-1 is less than or equal to 100 psf, with the exception of areas occupied as places of public assembly.
- 2. In combinations 2, 4, and 5, the companion load S shall be taken as either the flat roof snow load ( $p_f$ ) or the sloped roof snow load ( $p_s$ )
- 3. In IBC 1605.2, S in combination 5 shall be 0.7 for roof configurations (such as saw tooth) that do not shed snow off the structure.
- Section 2.3.3 : Load Combinations Including Flood Load. When a structure is located in a flood zone (Section 5.3.1), the following load combinations shall be considered in addition to the basic combinations in Section 2.3.2:
- 1. In V-Zones or Coastal A-Zones, 1.0W in combinations 4 and 6 shall be replaced by 1.0W + 2.0Fa.
- 2. In noncoastal A-Zones, 1.0W in combinations 4 and 6 shall be replaced by 0.5W + 1.0Fa.
- Section 2.3.4 : Load Combinations Including Atmospheric Ice Loads. When a structure is subjected to atmospheric ice and wind-on-ice loads, the following load combinations shall be considered:
- 1. 0.5(Lr or S or R) in combinatoin 2 shall be replaced by 0.2Di + 0.5S.
- 2. 1.0W + 0.5(Lr or S or R) in combination 4 shall be replaced by Di + Wi + 0.5S.
- 3. 1.0W in combination 6 shall be replaced by Di + Wi.

#### Symbols as used in calculations

- $D_1$  = dead load;
- $L_f$  = live load;
- $L_r$  = roof live load;
- $S_1$  = balanced snow
- $S_2$  = unbalanced snow
- $W_1$  = lateral wind +x (perpendicular to ridge line with overpressure)
- $W_2$  = lateral wind +x (perpendicular to ridge line with overpressure)
- $W_3$  = longitudinal wind +z (parallel to ridge line with underrpressure)
- $W_4$  = longitudinal wind +z (parallel to ridge line with underpressure)
- $W_5$  = lateral wind -x (perpendicular to ridge line with overpressure)
- $W_6$  = lateral wind -x (perpendicular to ridge line with overpressure)
- $W_7$  = longitudinal wind -z (parallel to ridge line with underrpressure)
- $W_8$  = longitudinal wind -z (parallel to ridge line with underpressure)

 $W_m$  = minimum design wind load

#### Combinations as applied in calculations :

Com	ipinations as applied in calculations :		
1.01	1.4D <sub>1</sub>	4.01	1.2D <sub>1</sub> + 1.0L <sub>f</sub> + 0.5L <sub>r</sub> + 1.0W <sub>1</sub>
2.01		.02	1.2D <sub>1</sub> +1.0L <sub>f</sub> + 0.5L <sub>r</sub> + 1.0W <sub>2</sub>
2.01	$12D_1 + 1.6L_f + 0.5L_f$	.03	1.2D <sub>1</sub> + 1.0L <sub>f</sub> + 0.5L <sub>r</sub> + 1.0W <sub>3</sub>
.02 .03	$12D_1 + 1.6L_f + 0.5S_1$	.04	1.2D <sub>1</sub> + 1.0L <sub>f</sub> + 0.5L <sub>r</sub> + 1.0W <sub>4</sub>
.03	12D <sub>1</sub> +1.6L <sub>f</sub> +0.5S <sub>2</sub>	.05	1.2D <sub>1</sub> + 1.0L <sub>f</sub> + 0.5L <sub>r</sub> + 1.0W <sub>5</sub>
3.01	1.2D <sub>1</sub> + 1.6L <sub>r</sub> + 1.0L <sub>f</sub>	.06	1.2D <sub>1</sub> + 1.0L <sub>f</sub> + 0.5L <sub>r</sub> + 1.0W <sub>6</sub>
.02	1.2D <sub>1</sub> + 1.6L <sub>r</sub> + 0.5W <sub>1</sub>	.07	1.2D <sub>1</sub> + 1.0L <sub>f</sub> + 0.5L <sub>r</sub> + 1.0W <sub>7</sub>
.03	1.2D <sub>1</sub> + 1.6L <sub>r</sub> + 0.5W <sub>2</sub>	.08	1.2D <sub>1</sub> + 1.0L <sub>f</sub> + 0.5L <sub>r</sub> + 1.0W <sub>8</sub>
.04	1.2D <sub>1</sub> + 1.6L <sub>r</sub> + 0.5W <sub>3</sub>	.09	1.2D <sub>1</sub> + 1.0L <sub>f</sub> + 0.5L <sub>r</sub> + 1.0W <sub>m</sub>
.05	1.2D <sub>1</sub> + 1.6L <sub>r</sub> + 0.5W <sub>4</sub>	.10	1.2D <sub>1</sub> + 1.0L <sub>f</sub> + 0.5S <sub>1</sub> + 1.0W <sub>1</sub>
.06	1.2D <sub>1</sub> + 1.6L <sub>r</sub> + 0.5W <sub>5</sub>	.11	$1.2D_1 + 1.0L_f + 0.5S_1 + 1.0W_2$
.07	1.2D <sub>1</sub> + 1.6L <sub>r</sub> + 0.5W <sub>6</sub>	.12	$1.2D_1 + 1.0L_f + 0.5S_1 + 1.0W_3$
.08	1.2D <sub>1</sub> + 1.6L <sub>r</sub> + 0.5W <sub>7</sub>	.13	1.2D <sub>1</sub> + 1.0L <sub>f</sub> + 0.5S <sub>1</sub> + 1.0W <sub>4</sub>
.09	1.2D <sub>1</sub> + 1.6L <sub>r</sub> + 0.5W <sub>8</sub>	.14	1.2D <sub>1</sub> + 1.0L <sub>f</sub> + 0.5S <sub>1</sub> + 1.0W <sub>5</sub>
.10	1.2D <sub>1</sub> + 1.6L <sub>r</sub> + 0.5W <sub>m</sub>	.15	$1.2D_1 + 1.0L_f + 0.5S_1 + 1.0W_6$
.11	1.2D <sub>1</sub> + 1.6S <sub>1</sub> + 1.0L <sub>f</sub>	.16	1.2D <sub>1</sub> + 1.0L <sub>f</sub> + 0.5S <sub>1</sub> + 1.0W <sub>7</sub>
.12	1.2D <sub>1</sub> + 1.6S <sub>1</sub> + 0.5W <sub>1</sub>	.17	1.2D <sub>1</sub> + 1.0L <sub>f</sub> + 0.5S <sub>1</sub> + 1.0W <sub>8</sub>
.13	1.2D <sub>1</sub> + 1.6S <sub>1</sub> +0.5W <sub>2</sub>	.18	$1.2D_1 + 1.0L_f + 0.5S_1 + 1.0W_m$
.14	1.2D <sub>1</sub> +1.6S <sub>1</sub> +0.5W <sub>3</sub>	.19	$1.2D_1 + 1.0L_f + 0.5S_2 + 1.0W_1$
.15	1.2D <sub>1</sub> +1.6S <sub>1</sub> +0.5W <sub>4</sub>	.20	$1.2D_1 + 1.0L_f + 0.5S_2 + 1.0W_2$
.16	1.2D <sub>1</sub> + 1.6S <sub>1</sub> + 0.5W <sub>5</sub>	.21	$1.2D_1 + 1.0L_f + 0.5S_2 + 1.0W_3$
.17	1.2D <sub>1</sub> + 1.6S <sub>1</sub> +0.5W <sub>6</sub>	.22	$1.2D_1 + 1.0L_f + 0.5S_2 + 1.0W_4$
.18	1.2D <sub>1</sub> +1.6S <sub>1</sub> +0.5W <sub>7</sub>	.23	$1.2D_1 + 1.0L_f + 0.5S_2 + 1.0W_5$
.19	1.2D <sub>1</sub> + 1.6S <sub>1</sub> + 0.5W <sub>8</sub>	.24	$1.2D_1 + 1.0L_f + 0.5S_2 + 1.0W_6$
.20	1.2D <sub>1</sub> + 1.6S <sub>1</sub> + 0.5W <sub>m</sub>	.25	$1.2D_1 + 1.0L_f + 0.5S_2 + 1.0W_7$
.21	1.2D <sub>1</sub> +1.6S <sub>2</sub> +1.0L <sub>f</sub>	.26	$1.2D_1 + 1.0L_f + 0.5S_2 + 1.0W_8$
.22	$1.2D_1 + 1.6S_2 + 0.5W_1$	.27	$1.2D_1 + 1.0L_f + 0.5S_2 + 1.0W_M$
.23	1.2D <sub>1</sub> +1.6S <sub>2</sub> +0.5W <sub>2</sub>		
.24	$1.2D_1 + 1.6S_2 + 0.5W_3$	6.01	0.9D <sub>1</sub> + 1.0W <sub>1</sub>
.25	1.2D <sub>1</sub> + 1.6S <sub>2</sub> + 0.5W <sub>4</sub>	.02	0.9D <sub>1</sub> + 1.0W <sub>2</sub>
.26	1.2D <sub>1</sub> + 1.6S <sub>2</sub> + 0.5W <sub>5</sub>	.03	0.9D <sub>1</sub> + 1.0W <sub>3</sub>
.27	$1.2D_1 + 1.6S_2 + 0.5W_6$	.04	0.9D <sub>1</sub> + 1.0W <sub>4</sub>
.28	1.2D <sub>1</sub> +1.6S <sub>2</sub> +0.5W <sub>7</sub>	.05	0.9D <sub>1</sub> + 1.0W <sub>5</sub>
.29	1.2D <sub>1</sub> +1.6S <sub>2</sub> +0.5W <sub>8</sub>	.06	0.9D <sub>1</sub> + 1.0W <sub>6</sub>
.30	1.2D <sub>1</sub> +1.6S <sub>2</sub> +0.5W <sub>m</sub>	.07	0.9D <sub>1</sub> + 1.0W <sub>7</sub>
5.01	1.2D <sub>1</sub> + 1.0L <sub>f</sub> + 0.2S <sub>1</sub>	.08	0.9D <sub>1</sub> + 1.0W <sub>8</sub>
.02	$12D_1 + 1.0L_f + 0.2S_2$	.09	0.9D <sub>1</sub> + 1.0W <sub>m</sub>
	1 1 2		

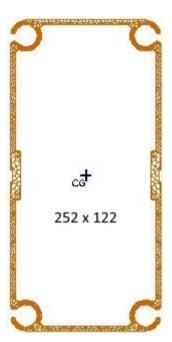


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#### 04a. Profile Design-Main Frame

#### **Section Properties :**

E = 10100·ksi	Table 3.3-1				
n <sub>u</sub> = 1.95	Table 3.4-1				
d = 9.921 · in	$b = 4.803 \cdot in$	Shape dimensions			
$b_w = 3.071 \cdot in$	$t_w = 0.157 \cdot in$				
$b_f = 2.677 \cdot in$	$t_{\rm f} = 0.16 \cdot in$				
$A_g = 5.521 \cdot in^2$		Cross-sectional area of Shape			
$I_x = 68.35 \cdot in^4$	$I_y = 22.21 \cdot in^4$	Moment of inertia			
$S_x = 13.78 \cdot in^3$	$S_y = 9.25 \cdot in^3$	Section Modulus			
$r_x = 3.52 \cdot in$	$r_y = 2.01 \cdot in$	Radius of Gyration			
$J = 43.27 \cdot in^4$		Torsional constant			
K <sub>x</sub> := 1.0	K <sub>y</sub> := 0.7	Factor for buckling			
$L_x = 129 \cdot in$	$L_y = 129 \cdot in$	Length for buckling			
$L_b := L_y$		Length between Bracing Points			



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#### **Selected Ratios :**

 $\frac{b_{w}}{t_{w}} = 19.5 \qquad \frac{b_{f}}{t_{f}} = 17 \qquad \frac{K_{x} \cdot L_{x}}{r_{x}} = 36.7 \qquad \frac{K_{y} \cdot L_{y}}{r_{y}} = 45 \qquad \frac{L_{b} \cdot S_{x}}{0.5\sqrt{I_{y} \cdot J}} = 114.7$ 

The following allowable stresses are based on values from the "2005 Aluminum Design Manual"

#### Allowable Axial Stress:

<u>Specification 3.4.1 - Tension, axial</u> : Any tension member.	$F_{3.4.1} = 32.3 \cdot ksi$
Specification 3.4.7 - Compression in Columns: All columns.	$F_{3.4.7x} = 25.98 \cdot ksi$ $F_{3.4.7y} = 32.22 \cdot ksi$
Specification 3.4.9 - Compression in Column Elements: Flat elements supported on both edges.	$F_{3.4.9} = 30.31 \cdot ksi$
Allowable Axial Stress:	$F_a = 25.98 \cdot ksi$ Use in Eq. 4.1.1-1
	$F_{ao} = 30.31 \text{ ksi}$ Use in Eq. 4.1.1-2
	$F_{ex} = 63.46 \cdot ksi$ $F_{ey} = 40.47 \cdot ksi$
	City of Dublin

Allowable Bending Stress: Specification 3.4.2 - Tension in Beams, extreme fibre, net section: Flat elements in uniform tension (flanges).	$F_{3.4.2} = 32.3 \cdot ksi$
<u>Specification 3.4.14 - Compression in Beams, gross section.</u> : Tubular shapes.	$F_{3.4.14} = 29.88 \cdot ksi$
<u>Specification 3.4.16 - Compression in Beams, gross section</u> : Flat elements supported on both edges.	$F_{3.4.16} = 31.33 \cdot ksi$
<u>Specification 3.4.19 - Compression in Beams, elements</u> : Flat elements supported on both edges with longitudinal stiffening.	$F_{3.4.19} = 43.22 \cdot ksi$
Allowable Bending Stress:	$F_{bx} = 29.88 \cdot ksi $ Use in Eq. 4.1.1-1 $F_{by} = 29.88 \cdot ksi $ & Eq. 4.1.1-2

#### Allowable Shear Stress:

Specification 3.4.20 - Shear in Elements, gross section:	$F_{3,4,20} = 19.2 \cdot ksi$
Unstiffened flat elements supported on both edges.	511120

#### **Actual Stress:**

Member ID = "	'ms23"	Load Case = "3.17-1.2D1+1.6S0+0.5W	/6"	
Cmx := 0.85	Cmy := 0.	$M_x = -63.57 \cdot kip \cdot in$	$M_y = 0.07 \cdot kip \cdot in$	$C = -8.76 \cdot kip$
		$f_{bx} := \left  \frac{M_x}{S_x} \right  = 4.61 \cdot ksi$	y	g
<u>Eq. 4.1.1-1</u> :	Eq1 :=	$\frac{f_{ac}}{F_{a}} + \frac{Cmx \cdot f_{bx}}{\left(1 - \frac{f_{ac}}{F_{ex}}\right) \cdot F_{bx}} + \frac{Cmy \cdot f_{by}}{\left(1 - \frac{f_{ac}}{F_{ey}}\right) \cdot F_{by}}$	= 0.2 Eq1 is less that	n or equal to $1.0 = "OK"$
<u>Eq. 4.1.1-2</u> :		$\frac{f_{ac}}{F_{ao}} + \frac{f_{bx}}{F_{bx}} + \frac{f_{by}}{F_{by}} = 0.21$		n or equal to $1.0 = "OK"$
Member ID = "	'ms25"	Load Case = "6.05-0.9D1+1.0W5"		
		$M_x = -140.86 \cdot kip \cdot in$	$M_y = 0.03 \cdot kip \cdot in$	$T = 6.65 \cdot kip$
		$f_{bx} := \left  \frac{M_x}{S_x} \right  = 10.22 \cdot ksi$	$f_{by} := \left  \frac{M_y}{S_y} \right  = 0 \cdot ksi$	$f_{at} := \frac{T}{A_g} = 1.2 \cdot ksi$
<u>Eq. 4.1.2-1</u> :	Eq3 :=	$\frac{f_{at}}{F_{3.4.1}} + \frac{f_{bx}}{F_{bx}} + \frac{f_{by}}{F_{by}} = 0.38$	Eq3 is less than or eq	ual to 1.0 = "OK"

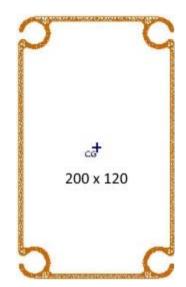


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#### 04b-Profile Design-Gable Uprights

#### **Section Properties :**

$E = 10100 \cdot ksi$	Table 3.3-1				
n <sub>u</sub> = 1.95	Table 3.4-1				
$d = 7.874 \cdot in$	$b = 4.724 \cdot in$	Shape dimensions			
$b_w = 5.846 \cdot in$	$t_w = 0.118 \cdot in$				
$b_f = 2.638 \cdot in$	$t_{\rm f} = 0.12 \cdot in$				
$A_g = 3.495 \cdot in^2$		Cross-sectional area of Shape			
$I_x = 31.56 \cdot in^4$	$I_y = 12.91 \cdot in^4$	Moment of inertia			
$S_x = 8.02 \cdot in^3$	$S_y = 5.46 \cdot in^3$	Section Modulus			
$r_x = 3.01 \cdot in$	$r_y = 1.92 \cdot in$	Radius of Gyration			
$J = 22.65 \cdot in^4$		Torsional constant			
K <sub>x</sub> := 1.0	K <sub>y</sub> := 0.7	Factor for buckling			
$L_x = 272 \cdot in$	$L_y = 208 \cdot in$	Length for buckling			
$L_b := L_y$		Length between Bracing Points			



#### **Selected Ratios :**

 $\frac{b_{w}}{t_{w}} = 49.5 \qquad \frac{b_{f}}{t_{f}} = 22.3 \qquad \frac{K_{x} \cdot L_{x}}{r_{x}} = 90.5 \qquad \frac{K_{y} \cdot L_{y}}{r_{y}} = 75.8 \qquad \frac{L_{b} \cdot S_{x}}{0.5\sqrt{I_{y} \cdot J}} = 195$ 

The following allowable stresses are based on values from the "2005 Aluminum Design Manual"

#### Allowable Axial Stress:

Specification 3.4.1 - Tension, axial: Any tension member.	$F_{3.4.1} = 32.3 \cdot ksi$	l		
Specification 3.4.7 - Compression in Columns: All columns.	$F_{3.4.7x} = 9.95 \cdot ks$	$F_{3.4.7x} = 9.95 \cdot ksi$		
Air columns.	$F_{3.4.7y} = 13.53 \cdot ksi$			
Specification 3.4.9 - Compression in Column Elements: Flat elements supported on both edges.	$F_{3.4.9} = 16.43 \cdot k$	si		
Allowable Axial Stress:	$F_a = 9.95 \cdot ksi$	Use in Eq. 4.1.1-1		
	$F_{ao} = 16.43 \cdot ksi$	Use in Eq. 4.1.1-2		
	$F_{ex} = 9.95 \cdot ksi$	$F_{ey} = 13.53 \cdot ksi$		



Allowable Bending Stress: Specification 3.4.2 - Tension in Beams, extreme fibre, net section: Flat elements in uniform tension (flanges).	$F_{3.4.2} = 32.3 \cdot ksi$
<u>Specification 3.4.14 - Compression in Beams, gross section.</u> : Tubular shapes.	$F_{3.4.14} = 28.79 \cdot ksi$
<u>Specification 3.4.16 - Compression in Beams, gross section:</u> Flat elements supported on both edges.	$F_{3.4.16} = 29.15 \cdot ksi$
<u>Specification 3.4.19 - Compression in Beams, elements</u> : Flat elements supported on both edges with longitudinal stiffening.	$F_{3.4.19} = 43.22 \cdot ksi$
Allowable Bending Stress:	$F_{bx} = 28.79 \cdot ksi$ Use in Eq. 4.1.1-1 $F_{by} = 28.79 \cdot ksi$ & Eq. 4.1.1-2

#### Allowable Shear Stress:

Specification 3.4.20 - Shear in Elements, gross section:	$F_{3,4,20} = 16.11 \cdot ksi$
Unstiffened flat elements supported on both edges.	511120

#### **Actual Stress:**

Member ID =	"gv001" Load Cas	e = "3.15 - 1.2D1 + 1.6S0 + 0.5W4	."	
Cmx := 0.85	Cmy := 0.85	$M_x = -37.61 \cdot kip \cdot in$	$M_y = 3.09 \cdot kip \cdot in$	$C = -1.22 \cdot kip$
		$f_{bx} := \left  \frac{M_x}{S_x} \right  = 4.69 \cdot ksi$		
<u>Eq. 4.1.1-1</u> :	$Eq1 := \frac{f_{ac}}{F_a} + \frac{C}{\left(1 - \frac{F_{ac}}{F_a}\right)}$	$\frac{cmx \cdot f_{bx}}{F_{ex}} + \frac{Cmy \cdot f_{by}}{\left(1 - \frac{f_{ac}}{F_{ey}}\right) \cdot F_{by}} =$	= 0.2 Eq1 is less that	n or equal to $1.0 = "OK"$
<u>Eq. 4.1.1-2</u> :	$Eq2 := \frac{f_{ac}}{F_{ao}} + \frac{f_{bx}}{F_{bx}}$			n or equal to $1.0 = "OK"$
Member ID =	"gv001" Load Ca	se = "6.04 - 0.9D1 + 1.0W4"		
		$M_x = -75.22 \cdot kip \cdot in$	$M_y = 6.68 \cdot kip \cdot in$	$T = 0.16 \cdot kip$
		$f_{bx} := \left  \frac{M_x}{S_x} \right  = 9.38 \cdot ksi$	$f_{by} := \left  \frac{M_y}{S_y} \right  = 1.22 \cdot ksi$	$f_{at} := \frac{T}{A_g} = 0.05 \cdot ksi$
<u>Eq. 4.1.2-1</u> :	$Eq3 := \frac{f_{at}}{F_{3.4.1}} + \frac{f_b}{F_t}$	$\frac{x}{x} + \frac{f_{by}}{F_{by}} = 0.37$	Eq3 is less than or eq	ual to 1.0 = "OK"



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#### 05. Splice Design

#### Eave Splice Design :

Section Properties :

Materials of construction :	S235 Steel	
Modulus of elasticity	E = 29000 · ksi	
Cross-sectional area	$A_g = 6.467 \cdot in^2$	
Shape dimensions	$b_w = 9.528 \cdot in$	$b_f = 2.953 \cdot in$
	$t_{\rm w}=0.472\!\cdot\!in$	$t_{\rm f}=0.295\!\cdot\!in$
Moment of inertia, strong/weak axis	$I_x = 74.54 \cdot in^4$	$I_y = 14.74 \cdot in^4$
Section Modulus, strong/weak axis	$S_x = 15.65 \cdot in^3$	$S_y = 6.72 \cdot in^3$
Radius of Gyration, strong/weak axis	$r_x = 3.4 \cdot in$	$r_y = 1.51 \cdot in$

#### Chapter D - Design of Members for Tension

 $\varphi_t \cdot P_n \quad \mbox{ design compressive strength for LRFD design }$ 

#### where :

 $\label{eq:pn} \begin{array}{ll} \mbox{nominal tensile strength as determined according to Sections D2-D6} \\ \varphi_{t,gross} = 0.9 & \varphi_{t,net} = 0.75 & \mbox{for LRFD design} \end{array}$ 

#### Tensile yielding in the gross section

$P_{ny} = F_y \cdot A_g$	(D2-1)
$P_{ny} := F_y \cdot A_g = 220.42 \cdot kip$	

#### Tensile rupture in the net section

$P_{nr} = F_y \cdot A_e$	(D2-2)
$P_{nr} := F_u \cdot A_e = 337.67 \cdot kip$	

#### Design tensile strength / Allowable tensile strength

 $\phi P_{nt} = 198.38 \cdot kip$  for LRFD design tensile strength



#### Chapter E - Design of Members for Compression

$\varphi_c \cdot P_n$ des	sign compressive strength for LRFD design
where :	
P <sub>n</sub>	nominal compressive strength as determined according to Sections E3-E7
$\phi_c = 0.$	9 for LRFD design
L	laterally unbraced length of the member, in (mm)
r	governing radius of gyration, in (mm)
Κ	effective length factor determined in accordance with Section C2

#### E3 - Compressive strength for flexural buckling of members without slender elements

$$P_n = F_{cr} A_g$$
(E3-1)

$$F_{e} := \frac{\pi^{2} \cdot E}{\left(\frac{K \cdot L}{r}\right)^{2}} = 59.17 \cdot ksi$$
(E3-4)

$$F_{cr} := if \left[ \frac{K \cdot L}{r_{y}} \le 4.71 \cdot \sqrt{\frac{E}{F_{y}}}, \left( 0.688 \frac{F_{y}}{F_{e}} \right) \cdot F_{y}, 0.877 \cdot F_{e} \right] = 27.48 \cdot ksi$$
(E3-2),
(E3-3)

$$P_n := F_{cr} \cdot A_g = 177.71 \cdot kip$$

#### Design compressive strength / Allowable compressive strength

#### $\Phi P_{ns} = 159.93 \text{ kin}$ for LRFD design compressive strength Chapter F - Design of Members for Flexure

#### F1. General Provisions

$\varphi_b{\cdot}M_n$	design flexural strength for LRFD design
where:	
M <sub>n</sub>	nominal flexural strength as determined according to Sections F2-F10

$$\varphi_b = 0.90 \qquad \qquad \text{for LRFD design}$$

#### F7. Rectangular HSS members

Yielding

$$M_{ny} := F_y Z_x = 682.36 \text{ kip} \text{ in}$$

$$M_p := F_y Z_x$$
(F7-1)



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#### Flange Local Buckling

For compact section, the limit state of flange local buckling does not apply

For noncompact sections

$$M_{n} := \min \left[ M_{p} - \left( M_{p} - F_{y} \cdot S_{x} \right) \cdot \left( 3.57 \cdot \frac{b}{t_{d}} \cdot \sqrt{\frac{F_{y}}{E}} - 4.0 \right), M_{p} \right] = 682.36 \cdot \text{kip} \cdot \text{in}$$
 (F7-2)

For sections with slender walls

$$b_{e} := 1.92 \cdot t_{d} \cdot \sqrt{\frac{E}{F_{y}}} \cdot \left(1 - \frac{0.38}{\frac{b}{t_{d}}} \cdot \sqrt{\frac{E}{F_{y}}}\right) = -15.98 \cdot in$$

$$S_{eff} := if \left[b_{e} < b, \frac{b_{e} \cdot h^{3} - (b_{e} - 2 \cdot t_{d}) \cdot (h - 2 \cdot t_{d})^{3}}{6 \cdot h}, S_{x}\right]$$

$$M_{n} := F_{y} \cdot S_{eff} = -1737.01 \cdot kip \cdot in$$

Flange Section Status = "The flange section of the rectangular HSS is compact since b/t = 3.72"

 $M_{nfb} = 999999999 \cdot kip \cdot in$ 

#### Web Local Buckling

For compact section, the limit state of web local buckling does not apply

For noncompact sections

$$M_{n} := \min \left[ M_{p} - \left( M_{p} - F_{y} \cdot S_{x} \right) \cdot \left( 3.05 \cdot \frac{h}{t_{d}} \cdot \sqrt{\frac{F_{y}}{E}} - 0.738 \right), M_{p} \right] = 454.56 \cdot \text{kip} \cdot \text{in}$$

Web Section Status = "The web section of the rectangular HSS is compact since h/t = 18.68"

#### Design Flexural Strength

 $\phi M_n = 614.12 \cdot kip \cdot in$  for LRFD design compressive strength

#### Stresses in Splice :

The connection splice is considered to carry the entire moment where the roof and column profiles meet.

Member ID = "mr20"Load Case = "3.17-1.2D1+1.6S0+0.5W6"  $M_x = -96.15 \cdot \text{kip} \cdot \text{in}$   $V = 1.86 \cdot \text{kip}$   $C = -8.88 \cdot \text{kip}$ 

Stress interaction on the solice :

ss interaction on the solice :  

$$IE := if \left[ \frac{|C|}{\phi P_{nc}} \ge 0.2, \frac{|C|}{\phi P_{nc}} + \frac{8}{9} \cdot \left( \frac{|M_x|}{\phi M_n} + \frac{|M_y|}{\phi M_n} \right), \frac{|C|}{2 \cdot \phi P_{nc}} + \left( \frac{|M_x|}{\phi M_n} + \frac{|M_y|}{\phi M_n} \right) \right] = 0.18$$

$$IE \text{ is less than or equal to } 1.0 = "OK"$$

Member ID = "mr20"Load Case = "3.17-1.2D1+1.6S0+0.5W6"  $M_x = -96.15 \cdot \text{kip} \cdot \text{in}$  V = 1.86 · kip

Stress interaction on the splice :

$$IE := if\left[\frac{T}{\phi P_{nt}} \ge 0.2, \frac{T}{\phi P_{nt}} + \frac{8}{9} \cdot \left(\frac{\left|M_{x}\right|}{\phi M_{n}} + \frac{\left|M_{y}\right|}{\phi M_{n}}\right), \frac{T}{2 \cdot \phi P_{nt}} + \left(\frac{\left|M_{x}\right|}{\phi M_{n}} + \frac{\left|M_{y}\right|}{\phi M_{n}}\right)\right] = 0.35$$
  
IE is less than or equal to 1.0

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#### Peak Splice Design : Section Properties :

Materials of construction :	S355 Steel	
Modulus of elasticity	E = 29000 · ksi	
Cross-sectional area	$A_g = 6.467 \cdot in^2$	
Shape dimensions	$b_w = 9.528 \cdot in$	$b_f = 2.953 \cdot in$
	$t_w = 0.472 \cdot in$	$t_{\rm f}=0.295\!\cdot\!in$
Moment of inertia, strong/weak axis	$I_x = 74.54 \cdot in^4$	$I_y = 14.74 \cdot in^4$
Section Modulus, strong/weak axis	$S_x = 15.65 \cdot in^3$	$S_y = 6.72 \cdot in^3$
Radius of Gyration, strong/weak axis	$r_x = 3.4 \cdot in$	$r_y = 1.51 \cdot in$

#### Stresses in Splice :

#### The connection splice is considered to carry the entire moment where the main profiles meet. Member ID = "mr3" Load Case = "3.26-1.2D1+1.6S6+0.5W6"

$$M_x = 12.28 \cdot kip \cdot in$$
  $V = -0.46 \cdot kip$   $C = -0.97 \cdot kip$ 

Stress interaction on the splice :

$$IE := if\left[\frac{|C|}{\Phi P_{nc}} \ge 0.2, \frac{|C|}{\Phi P_{nc}} + \frac{8}{9} \cdot \left(\frac{|M_x|}{\Phi M_n} + \frac{|M_y|}{\Phi M_n}\right), \frac{|C|}{2 \cdot \Phi P_{nc}} + \left(\frac{|M_x|}{\Phi M_n} + \frac{|M_y|}{\Phi M_n}\right)\right] = 0.02$$

IE is less than or equal to 1.0 = "OK"

$$\begin{split} \text{Member ID} &= \text{"mr3"} & \text{Load Case} = \text{"3.26-1.2D1+1.6S6+0.5W6"} \\ & M_x = 30.03 \cdot \text{kip} \cdot \text{in} & \text{V} = -0.6 \cdot \text{kip} & \text{T} = 1.24 \cdot \text{kip} \\ \text{Stress interaction on the splice} : \\ & \text{IE} := \text{if} \Bigg[ \frac{T}{\varphi P_{nt}} \geq 0.2, \frac{T}{\varphi P_{nt}} + \frac{8}{9} \cdot \Bigg( \frac{\left| M_x \right|}{\varphi M_n} + \frac{\left| M_y \right|}{\varphi M_n} \Bigg), \frac{T}{2 \cdot \varphi P_{nt}} + \Bigg( \frac{\left| M_x \right|}{\varphi M_n} + \frac{\left| M_y \right|}{\varphi M_n} \Bigg) \Bigg] = 0.05 \end{split}$$

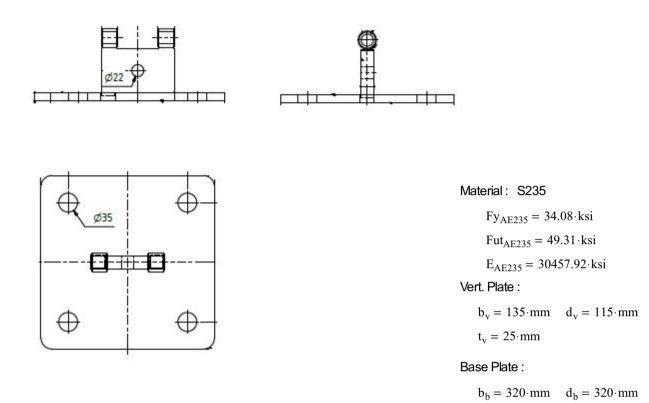
IE is less than or equal to 1.0 = "OK"



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 $t_b = 15 \cdot mm$ 

#### 06. Base plate Design



#### Vertical plates :

Section Properties (single vertical plate):

$$A_v := b_v \cdot t_v = 5.23 \cdot in^2$$
  $S_{vx} := \frac{t_v \cdot b_v^2}{6} = 4.63 \cdot in^3$   $S_{vy} := \frac{b_v \cdot t_v^2}{6} = 0.86 \cdot in^3$ 

Allowable Stress :

 $\sigma_{allowable} := \phi_b \cdot Fy_{AE235} = 30.68 \cdot ksi$ 



#### Actual Stress :

Moment arm above Section :  $d_{\rm B} = 9.45 \cdot in$ 

 $LoadCase_0 = "6.02-0.9D1+1.0W2"$ 

$$\sigma \coloneqq \left| \frac{V_0}{2 \cdot A_v} + \frac{0.5 \cdot H_0 \cdot d_B}{2 \cdot S_{vy}} \right| = 6.04 \cdot ksi$$

 $LoadCase_1 = "6.06-0.9D1+1.0W6"$ 

$$\sigma := \left| \frac{\mathrm{V}_{1}}{(2) \cdot \mathrm{A}_{\mathrm{v}}} - \frac{0.5 \cdot \mathrm{H}_{1} \cdot \mathrm{d}_{\mathrm{B}}}{2 \cdot \mathrm{S}_{\mathrm{vy}}} \right| = 7.45 \cdot \mathrm{ksi}$$

#### Bending of Base Plate :

Allowable Stress :

 $\sigma_{\text{allowable}} := \phi_b \cdot Fy_{\text{AE355}} = 46.34 \cdot ksi$ 

Surface area of base plate :  $A := L \cdot W = 158.72 \cdot in^2$ 

The reaction forces act on a distance "d" above the bottom side of plate:

 $LoadCase_0 = "3.17 - 1.2D1 + 1.6S0 + 0.5W6"$ 

These forces result in the following pressure under the baseplate:

$$f_{max} := \frac{V_0}{A} + \frac{H_0 \cdot d \cdot (6)}{L \cdot W^2} \qquad f_{max} = 383.78 \cdot \frac{kN}{m^2}$$

$$f_{max} = 0.056 \cdot ksi$$

$$f_{min} := \frac{V_0}{A} - \frac{H_0 \cdot d \cdot (6)}{L \cdot W^2} \qquad f_{min} = 2.7 \cdot \frac{kN}{m^2}$$

$$f_{min} = 0 \cdot ksi$$
Pressure under the BasePlate
$$f_{min} = 0 \cdot ksi$$
The pressure  $f_A$  equals:
$$f_A := f_{max} - \left(\left|f_{max}\right| + \left|f_{min}\right|\right) \cdot \frac{153 \cdot mm}{a^2} \qquad f_A = 186.7 \cdot \frac{kN}{a} \qquad f_A = 0.03 \cdot ksi$$

Sec

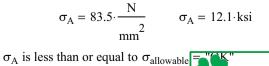
The pressure 
$$f_A$$
 equals:  $f_A := f_{max} - (|f_{max}| + |f_{min}|) \cdot \frac{153 \cdot mm}{300 \cdot mm}$   $f_A = 186.7 \cdot \frac{kN}{m^2}$   $f_A = 0.03 \cdot ksi$ 

The moment resulting from the pressure under the plate equals :

$$M_{A} := \left(\frac{f_{max} + f_{A}}{2}\right) \cdot 153 \cdot mm \cdot \left(\frac{153 \cdot mm}{2} \cdot 300 \cdot mm\right) \qquad \qquad M_{A} = 1 \cdot kN \cdot m \qquad \qquad M_{A} = 8.9 \cdot kip \cdot in$$
  
e actual stress equals : 
$$\sigma_{A} := \frac{M_{A} \cdot 6}{L \cdot T^{2}} \qquad \qquad \sigma_{A} = 83.5 \cdot \frac{N}{mm^{2}} \qquad \qquad \sigma_{A} = 12.1 \cdot ksi$$

The actual stress equals :

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 $d = 225 \cdot mm$ 

 $H_0 = -2.09 \cdot kip$   $V_0 = -2.99 \cdot kip$ 

 $H_1 = 2.56 \cdot kip$   $V_1 = -4.18 \cdot kip$ 

$$H_0 = 1.04 \cdot kip$$
  $V_0 = 4.45 \cdot kip$ 

 $\sigma$  is less than or equal to  $\sigma_{allowable} = "OK"$ 

 $\sigma$  is less than or equal to  $\sigma_{allowable} = "OK"$ 

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#### 7.Purlin-120x80x3

#### **Section Properties :**

Table 3.3-1	$E = 29000 \cdot ksi$	Cross-sectional area	$A_g = 1.77 \cdot in^2$	
Yield/Ultimate stresses	$F_y = 50 \cdot ksi$ $F_u = 65 \cdot ksi$	Moment of inertia	$I_x = 5.53 \cdot in^4$	$I_v = 2.97 \cdot in^4$
Shape dimensions	$h = 4.72 \cdot in  b = 3.15 \cdot in$			,
	$t = 0.12 \cdot in$	Section modulus	$S_x = 2.34 \cdot in^3$	$S_y = 1.88 \cdot in^2$
		Radius of gyration	$r_x = 1.79 \cdot in$	$r_y = 1.3 \cdot in$
			4	

Torsional constant

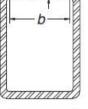
#### $J = 6.16 \cdot in^4$

Section is = "compact"

#### Table B4.1 Limiting Width-Thickness Ratios for Compression Elements

Case 12 Uniform compression in flanges of rectangular box and hollow structural sections of uniform thickness subject to bendina or compression.

$$b = 2.82 \cdot in \quad t = 0.12 \cdot in \quad b \ / \ t_d = 25.67 \qquad \lambda_p := 1.12 \cdot \sqrt{\frac{E}{F_y}} = 26.97 \qquad \lambda_r := 1.40 \cdot \sqrt{\frac{E}{F_y}} = 33.72$$



Case 13 Flexure in webs of rectangular HSS

h = 4.39 in t = 0.12 in h / t<sub>d</sub> = 40.01  $\lambda_p := 2.42 \cdot \sqrt{\frac{E}{F_v}} = 58.28 \quad \lambda_r := 5.70 \cdot \sqrt{\frac{E}{F_v}} = 137.27$ Section is = "compact"

#### Allowable Strength:

Chapter D - Design of Members for Tension	$P_c = 79.61 \cdot kip$
Chapter E - Design of Members for Compression	$P_c = 17.27 \cdot kip$
Chapter F - Design of Members for Flexure	$M_{cx} = 126.9 \cdot kip \cdot in$
	$M_{cy} = 96.21 \cdot kip \cdot in$

#### Actual Required Strength:

(worst case shown)

Member ID = "pl3"

Load Case = "6.04-0.9D1+1.0W4"

$$M_{rx} = 0 \cdot kip \cdot in \qquad M_{ry} = 0 \cdot kip \cdot in \qquad P_r = -4.31 \cdot kip$$
For  $\frac{P_r}{P_c} \ge 0.2 \qquad \frac{P_r}{P_c} + \frac{8}{9} \cdot \left(\frac{M_{rx}}{M_{cx}} + \frac{M_{ry}}{M_{cy}}\right) \le 1.0 \qquad (H1-1a)$ 
For  $\frac{P_r}{P_c} < 0.2 \qquad \frac{P_r}{P_c} + \left(\frac{M_{rx}}{P_c} + \frac{M_{ry}}{P_c}\right) \le 1.0 \qquad (H1-1b)$ 

$$P_{c} \qquad 2 \cdot P_{c} \qquad \left(M_{cx} \qquad M_{cy}\right)$$

$$IE := if \left[\frac{|P_{r}|}{P_{c}} \ge 0.2, \frac{|P_{r}|}{P_{c}} + \frac{8}{9} \cdot \left(\frac{|M_{rx}|}{M_{cx}} + \frac{|M_{ry}|}{M_{cy}}\right), \frac{|P_{r}|}{2 \cdot P_{c}} + \left(\frac{|M_{rx}|}{M_{cx}} + \frac{|M_{ry}|}{M_{cy}}\right)\right] = 0.25$$

$$IE := if \left[\frac{|P_{r}|}{P_{c}} \ge 0.2, \frac{|P_{r}|}{P_{c}} + \frac{8}{9} \cdot \left(\frac{|M_{rx}|}{M_{cx}} + \frac{|M_{ry}|}{M_{cy}}\right), \frac{|P_{r}|}{2 \cdot P_{c}} + \left(\frac{|M_{rx}|}{M_{cx}} + \frac{|M_{ry}|}{M_{cy}}\right)\right] = 0.25$$

IE is less than or equal to 1.0 = "OK"



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### 8. Bracing Cables

The roof bracing cables are constructed of 6x19 Galvanized EIPS Wire Rope.



The max factored load in a roof wind brace is  $T_{max} = 2900 \, lbf$ .

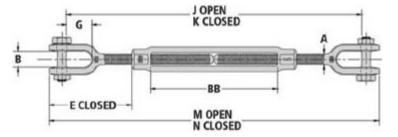
The nominal strength of  $\phi = 0.400 \text{ in}$  wire rope is  $T_{allow} = 17220 \text{ lbf}.$ 

Safety Factor := 
$$\frac{T_{allow} \cdot 90\%}{T_{max}} = 5.34$$

Rope Diameter		rength*,Tons Galvanized) EIPS	Appr Wt./	oximate Ft. (Lbs.)
(ln.)	IWRC	Fiber Core	IWRC	Fiber Core
1/4	3.40	3.02	0.116	0.105
5/10	5.27	4.67	0.18	0.164
9/8	7.55	6.71	0.26	0.236
7/18	102	9.09	0.35	0.32
1/2	133	11.8	0.46	0.42
9/4s	16.8	14.9	0.59	0.53
<del>5</del> 8	20.6	18.3	0.72	0.66
3/4	29.4	26.2	1.04	0.95
7/8	39.8	35.4	1.42	1.29
1	517	46.0	1.85	1.68
11/6	65.0	57.9	2.34	2.13
11/4	79.9	71.0	2.89	2.63
13/8	96.0	85.4	3.50	3.18
11/2	1140	101.0	4.16	3.78

USE a 6x19 Galvanized EIPS wire rope with a minimum diameter of  $\varphi=0.4000\,in$  .

Adjustment of the roof bracing cables is through turnbuckles.



The max factored load in a roof wind brace is  $T_{max} = 2900 \, \text{lbf}$ . The working strength of  $\phi = 0.750 \, \text{in}$  turnbuckle is  $T_{work} = 5200 \, \text{lbf}$ . The nominal strength of  $\phi = 0.750 \, \text{in}$  turnbuckle is  $T_{allow} = 26000 \, \text{lbf}$ .

Safety Factor := 
$$\frac{T_{allow}}{T_{max}} = 8.97$$

USE a turnbuckle with a minimum thread diameter of  $\varphi=0.7500\,in$  .

\* Proof Load is 2.5 Times Work Load Limit.

Thread Diameter & Take Up (Inches)	Work Load Limit (Lbs.)*	Unit Weight (Lbs.)
† 1/4 x 4	500	.37
† 5/16 x 4-1/2	800	.56
† 3/8 x 6	1200	.85
1/2 x 6	2200	1.82
1/2 x 9	2200	2.29
1/2 x 12	2200	2.71
5/8 x 6	<mark>3500</mark>	3.21
5/8 x 9	3500	3.95
5/8 x 12	3500	4.58
3/4 x 6	5200	4.80
3/4 x 9	5200	5.85
3/4 x 12	5200	6.72
3/4 x 18	5200	8.45
7/8 x 12	7200	9.37
7/8 x 18	7200	11 20
1 x 6	10000	IVA

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APPENDIX A FIGURES AND SKETCHES



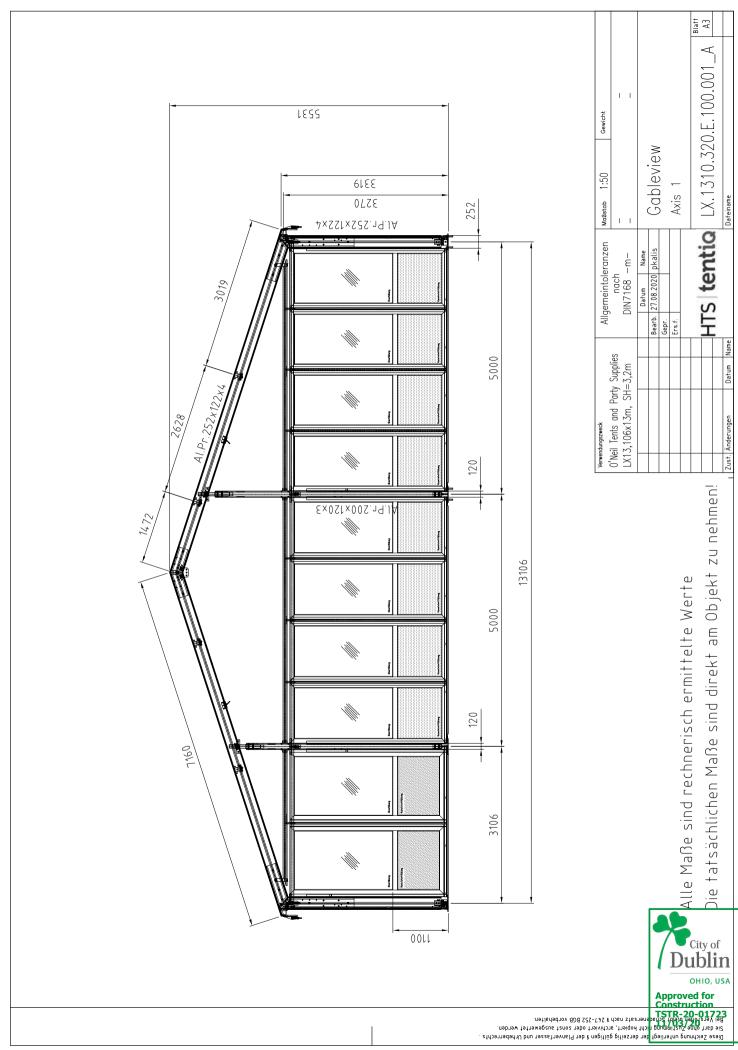
A1 - Appendix A-HTS Hoecker.xmcd

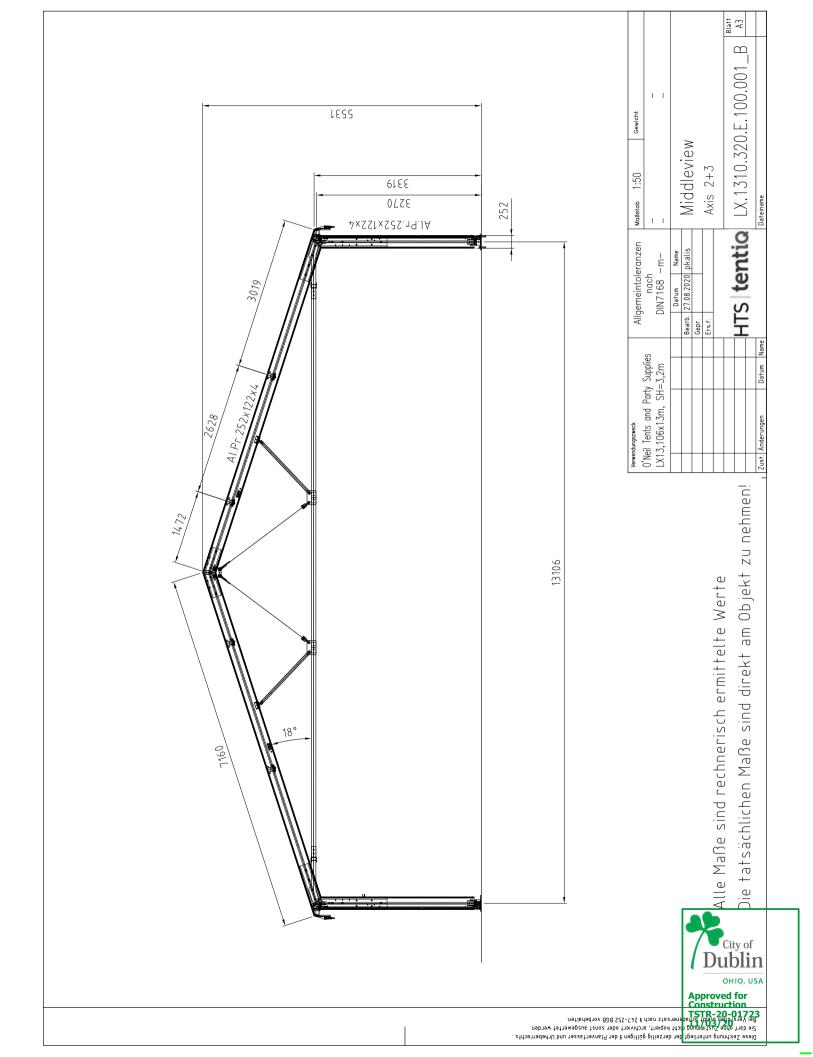
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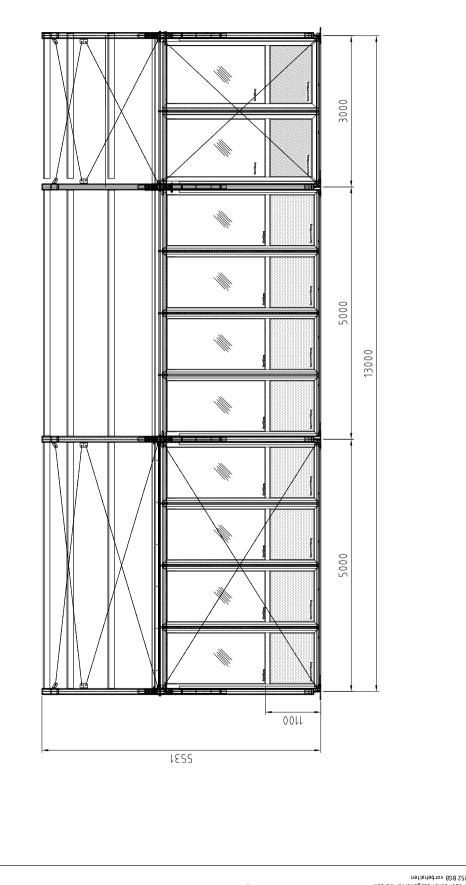




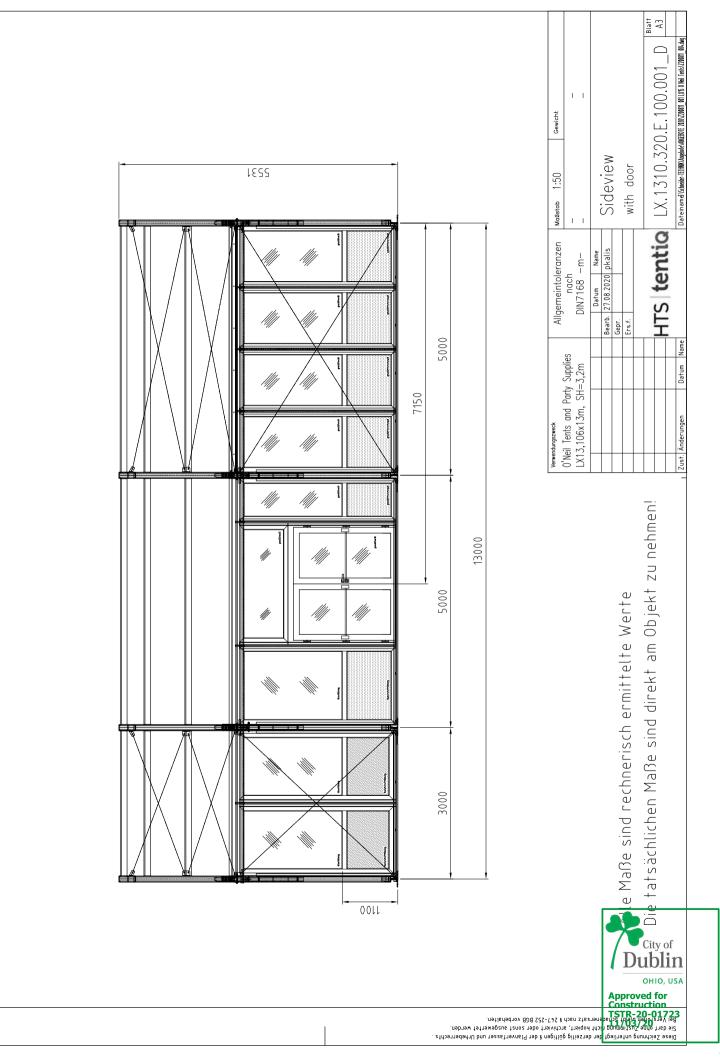
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verwendungszweck 0'Neil Tents and Party Supplies	LX15,106x15m, SH=5,2m							 Zust. Änderungen Datum Name
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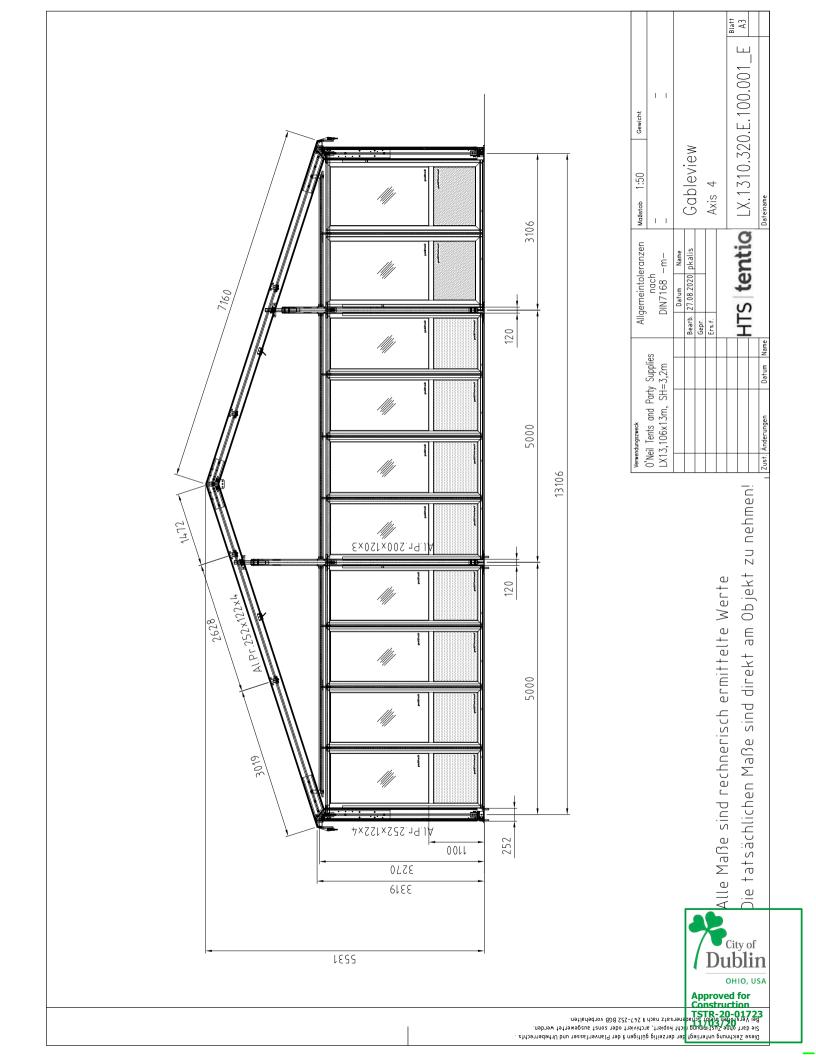
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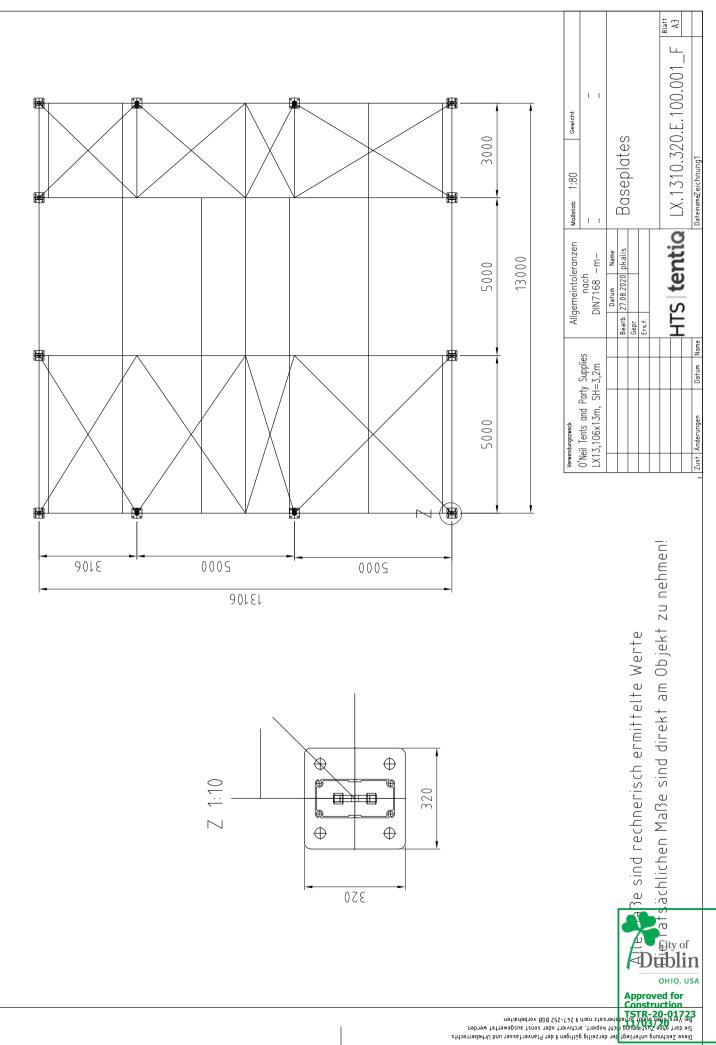
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# APPENDIX B COMPUTER MODEL INPUT



A2 - Appendix B-HTS Hoecker.xmcd

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A2 - Appendix B-HTS Hoecker.xmcd

00         13.25         31.95%         00			,⊐	Fix DX	Fix DY	Fix DZ	Fix RX		FIX RZ
2         74,41         31496/b         b0					No	No	No	No	No
11         1.1.5.7         3.145900         00					No	No	No	No	No
88         2003         313,900         00					NO	ON	ON ON	ON ON	NO
1.5         1.23         314.960         No					No	No	No	No	No
1.15       1.13.1       314.9610       No       No <td></td> <td></td> <td></td> <td></td> <td>No</td> <td>No</td> <td>No</td> <td>No</td> <td>No</td>					No	No	No	No	No
88         177.24         314.96/0         No					No	No	No	No	No
10.00         17.12.43         31.14.100         NO					No	No	No	No	No
1         1					No	No	No	No	No
15.5         15.10         7.1131100         NO					NO	ON ON	ON ON	ON ON	ON ON
00         152.8         5113100         N0					NO	No	N	N	N
38         74.41         51.18100         No					No	No	No	No	No
8.81         134.52         51181/0         No					No	No	No	No	No
38         205.21         51181N0         No					No	No	No	No	No
1.55         151.07         51.31.00         No					No	No	No	No	No
(3)         132.83         51131No         No					No	No	No	No	No
87         74-41         51131No         No					No	No	No	No	No
38         138.74 138.74         51131No 51131No         No         No <th< td=""><td></td><td></td><td></td><td></td><td>No</td><td>No</td><td>No</td><td>No</td><td>No</td></th<>					No	No	No	No	No
					No	No	No	No	No
1.58         2.06-/13         31131No         No	7				No	No	No	No	No
KkDX         Fix DX         Fix DX <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>No</td> <td>0N</td> <td>ON</td>							No	0N	ON
Kr DX     Fix DZ     Fix DZ     Fix RX     Fix RX     Fix RX       Yes     Yes     Yes     No     No     No     No       Yes     Yes     No     No     No     No     No       Yes     Yes     Yes     No     No     No <td></td> <td></td> <td></td> <td></td> <td>NO</td> <td>NO</td> <td>ON N</td> <td>NO</td> <td>NO NO</td>					NO	NO	ON N	NO	NO NO
KDX     Fix DX     Fix DZ     Fix RX	al Sunnorte				2	2.	2	2	2
Yes     Yes     Yes     No     No     No     No       Yes     Yes     No     No     No     No       Yes     No     No     No     No     N		X DX	Fix DY		Fix DZ	Fix RX	<u>تت</u>	×КҮ	Fix RZ
Mes     Mes     Mes     Mes     No     No     No       Yes     Yes     Nes     No     No     No     No     No       Yes     Yes     Nes     No     No     No     No     No       Yes     Yes     Nes     No     No     No     No     No       Yes     Yes     No     No     No     No     No     No       Yes     No     No     No     No     No     No     No       Yes     Yos     No     No     No     No <td>Yes</td> <td></td> <td></td> <td>Yes</td> <td></td> <td></td> <td></td> <td></td> <td></td>	Yes			Yes					
Yes     Yes     No     No     No     No       Yes     Yes     No     No     No     No     No       Yes     Yes     No     No     No     No     No       Yes     Yes     Yes     No     No     No     No       Yes     Yes     No     No     No     No     No       Yes     No     No     No     No     No     No       Yes     Yes     No     No     No     No     No       Yes     Yes     No     No     No     No       <		×	es	Yes		No	No	No	
New     New     No     No     No     No       Yes     Yes     No     No     No     No     No       Yes     Yes     Yes     No     No     No     No       Yes     Yes     No     No     No     No       Yes     No     No     No     No     No       Yes     Yes     No     No     No       Y		>	es	Yes		No	No	No	
New     New     New     No     No     No       Yes     Yes     No     No     No     No     No       Yes     Yes     Yes     No     No     No     No       Yes     Yes     Yes     No     No     No     No       Yes     Yes     No     No     No     No     No       Yes     No     No     No     No     No     No       Yes     No     No     No     No     No     No       Yes     No     No     No     No     No     No       Yes     Yes     No     No     No     No     No       Yes     No     No     No     No     No     No       Yes     No     No     No     No     No     No       Yes     Yes     No     No     No     No <td< td=""><td></td><td>× :</td><td>es</td><td>Yes</td><td></td><td>No</td><td>No :</td><td>8 2</td><td></td></td<>		× :	es	Yes		No	No :	8 2	
Mes     Mes     Mes     Mo     Mo       Yes     Yes     No     No     No     No       Yes     No     0.10     1.305.005     1     1       1010000100     0.33     0.10     1.305.005     1     1       290000000     0.23     0.10     1.305.005     1     1       1010000100     0.23     0.10     1.305.005     1     1       290000000     0.23     0.10     0.28     0.01     1     1       1     290000.00     0.23     0.02     1     1     1       1     1     1     1     1     1     1       1     1     1     1     1     1     1       1     1     1     1     1     1     1       1 <td></td> <td>~ &gt;</td> <td>es</td> <td>Yes</td> <td></td> <td>ON</td> <td>ON N</td> <td>ON ON</td> <td></td>		~ >	es	Yes		ON	ON N	ON ON	
Yes     Yes     No     No     No     No       Yes     Yes     No     No     No     No     No       Yes     No     No     No     No     No     No       Yes     Yes     No     No     No     No     No       Yes     Yes     No     No     No     No     No       Yes     Yes     Yes     No     No     No     No       Yes     Yes     Yes     Yes     No     No <td< td=""><td></td><td></td><td>es es</td><td>Yes</td><td></td><td>No</td><td>No</td><td>No</td><td></td></td<>			es es	Yes		No	No	No	
Yes     Yes     No     No     No     No       Yes     Yes     No     No     No     No     No       1010000100     0.33     0.10     1.30E-005     Dsi     1       290000000     0.23     0.10     1.30E-005     1     1       290000000     0.23     0.20     0.20     1.30E-005     1     1       290000000     0.23     0.10     5.39E-005     1     1       290000000     0.23     0.20     0.20     1.30E-005     1       290000000     0.23     0.20     0.20     1.30E-005     1       290000000     0.23     0.20     0.20     1.30E-005     1       29000000     0.20     0.20     0.20     1.30E-005     1       2900000     0.20     0.20     0.36E-005     1     1       2900000     0.20     0.20     5.61006     1     1 <td></td> <td></td> <td>S</td> <td>Yes</td> <td></td> <td>No</td> <td>No</td> <td>No</td> <td></td>			S	Yes		No	No	No	
West West Vest Vest Vest Vest Vest Vest Vest V		Σ.	es	Yes		No	No	No	
Mes     Mes     Mes     Mes     No     No     No       Miss     Yes     No     No     No     No     No       In10000000     0.33     0.10     1.30E.005     No     No       In10000000     0.33     0.10     1.30E.005     No       In10000000     0.23     0.10     1.30E.005     No       In10000000     0.23     0.10     1.30E.005     No       In10000000     0.23     0.00     0.23     0.10     1.30E.005       In100000000     0.23     0.00     0.23     0.10     1.30E.005       In100000000     0.23     0.00     0.23     0.10     1.1       In100000000     0.23     0.00     0.23     0.10     1.1       In100000000     0.23     0.00     0.23     0.10     1.1       In100000000     0.23     0.00     0.23     0.00     1.1		> :	es	Yes		No	No	No	
Inserticity, E         Poisson, v         Density, v         Thermal, a         Model         Model <t< td=""><td></td><td>~ &gt;</td><td>es</td><td>Yes</td><td></td><td>No</td><td>No</td><td>No</td><td></td></t<>		~ >	es	Yes		No	No	No	
Flasticity, E     Poisson, v     Density, v     Informal, a     Shear       1010000000     0.33     0.10     1.30E-005     1       290000000     0.29     0.00     6.39E-006     1       290000000     0.29     0.00     0.00     1       290000000     0.29     0.00     0.00     1       290000000     0.29     0.00     0.00     1       290000000     0.29     0.00     0.00     1       290000000     0.29     0.00     1     1       2900000000     0.29     0.00     1     1       2900000000     0.29     0.00     0.00     1       2900000000     0.29     0.00     0.00     1       290000000     0.29     0.00     1     1       290000000     0.29     0.00     1     1       20000000     0.29     0.00     1     1       20000000     1     1     1     1       200000000     1     1     1     1 <td></td> <td>E</td> <td>5</td> <td>5</td> <td></td> <td>DNI</td> <td>INO</td> <td>MO</td> <td></td>		E	5	5		DNI	INO	MO	
Elasticity, Minh/deg-F     Montani, a     Noment, a <t< td=""><td>laterials</td><td>ī</td><td>L</td><td></td><td>-</td><td>_</td><td></td><td>ī</td><td></td></t<>	laterials	ī	L		-	_		ī	
101000000         0.33         0.10         1.30E-005         1.30E-005           290000000         0.29         0.00         0.28         6.39E-005         1           290000000         0.29         0.00         6.39E-005         1         1           20005         0.29         0.00         0.00         5.38E/005         1         1           2005         Exclude         Exclude         Exclude         1	Name	Elast	icity, E Ssi	Poisson, v			ermal, a n/deg-F	Shodu Modu	ear Ilus, G Si
230000000     0.29     0.28     6.39E-006       290000000     0.29     0.29     0.00     6.39E-006       290000000     0.00     6.39E-006     5.39E-006       ef     codds     Exclude     Exclude	61-T6-E-All		10100000.00		0.33	0.10	1.30E-005		
2300000.00 0.29 0.00 6.39E-006 er Loads er Loads	TM A36		2900000.00		0.29	0.28	6.39E-006		1124031
File     Source     SetMvdght       File     Source     SetMvdght       File     Exclude     Exclude			2900000.00		0.29	0.00	6.39E-006		1124031
Source     SetMidght       er     Loads     Exclude       er     Exclude     Exclude </td <td>ervice Load Cases</td> <td></td> <td></td> <td></td> <td>_</td> <td></td> <td>_</td> <td></td> <td></td>	ervice Load Cases				_		_		
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HTS F173 13M

Table of Contents

Result Cases	
Na	Name
3.13-1.2D1+1.6S0+0.5W2	17
3.14-1.2D1+1.6S0+0.5W3	18
3.15-1.2D1+1.6S0+0.5W4	19
3.16-1.2D1+1.6S0+0.5W5	20
3.17-1.2D1+1.6S0+0.5W6	21
3.18-1.2D1+1.6S0+0.5W7	22
3.19-1.2D1+1.6S0+0.5W8	33
3.21-1.2D1+1.6S1+0.5W1	24
3.22-1.2D1+1.6S2+0.5W2	25
3.23-1.2D1+1.6S3+0.5W3	26
3.24-1.2D1+1.6S4+0.5W4	27
3.25-1.2D1+1.6S5+0.5W5	28
3.26-1.2D1+1.6S6+0.5W6	29
3.27-1.2D1+1.6S7+0.5W7	30
3.28-1.2D1+1.6S8+0.5W8	31
6.01-0.9D1+1.0W1	32
6.02-0.9D1+1.0W2	33
6.03-0.9D1+1.0W3	34
6.04-0.9D1+1.0W4	35
6.05-0.9D1+1.0W5	36
6.06-0.9D1+1.0W6	37
6.07-0.9D1+1.0W7	38



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# APPENDIX C COMPUTER MODEL OUTPUT



A3 - Appendix C-HTS Hoecker.xmcd

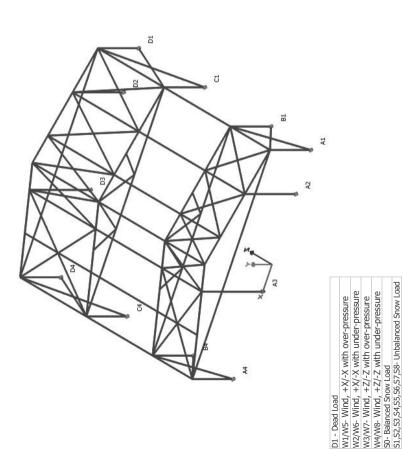
HTS tentiQ GmbH Hinter der SchlagmÃ1¼hle 1 63699 Kefenrod Germany

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A3 - Appendix C-HTS Hoecker.xmcd

A2 A2 82	kesuit case	X q	<u></u> 1	L P	MX Ib-in	MY Ib-in	MZ lb-in
	S6		940.55	0.05	0.00	0.00	0.00
	W1	-88.54	-1132.67	-0.08	00.00	0.00	0.0
	W2	-85.89	-688.20	-0.05	0.00	0.00	0.0
	W3 M2	90.07 05 AG	07.1002- 77.100C	-393./4	0.00	0.00	0.0
	WF5	02.09	-1476.34	80 0-	000	0.0	000
	W6	63.35	-981.50	-0.04	0.00	0.00	0.0
42	W7	-79.01	88.30	840.60	0.00	0.00	0.0
	W8	-68.95	414.64	196.82	00.00	0.00	0.00
	D1	0.13	27.42	0.00	00.00	0.00	0.0
	SO	3.91	847.49	0.02	0.00	0.00	0.0
43	21	10.38	1143.03	0.02	0.00	0.00	0.0
-	52	10.38	216.05	0.02	0.00	0.00	0.0
	<u>қ</u> у	-2.81	316.05	0.01	0.00	0.00	00.0
23	200	UC 22-	-1764 43	10'0-	00.0	00.0	0.0
	C/M	-74.38	-1221.55	0.00	00.0	0.0	0.0
	W3	73.40	-626.14	-605.87	0.00	0.00	0.00
	W4	69.71	-178.72	-1595.13	00.00	0.00	0.0
43	W5	50.28	-1170.50	-0.07	00.00	0.00	0.0
43	W6	53.10	-626.95	-0.05	00.00	0.00	0.00
	W7	-65.92	-1581.17	1293.49	0.00	0.00	0.0
	W8	-57.86	-1098.37	302.88	0.00	0.00	0.0
	10	-0.60	17.23	0.25	0.00	0.00	0.0
44	20	20.CC- 21.05-	242.90	1.40 1.40	0.0	0.00	0.00
	10	91.05-	459.31	1 40	00.0	000	000
44	55	-33.61	401.10	-0.53	0.00	0.00	0.0
	S6	-33.61	401.10	-0.53	0.00	0.00	0.00
	W1	-528.77	-859.23	-61.46	00.00	0.00	0.00
	W2	406.50	-381.72	-39.63	0.00	0.00	0.00
	W3	80.80	-1889.46	-530.37	0.00	0.00	0.00
44	VV4 IV/E	1/8.1U	-2091.42	411.00	0.00	0.00	0.00
44	M6	606.62	-742.35	-24.56	0.00	0.00	0.00
44	W7	404.65	202.76	407.74	0.00	0.00	0.00
	W8	-263.76	-36.88	95.21	0.00	0.00	0.00
	D1	25.91	281.56	0.61	0.00	0.00	0.00
	20	321.15	2737.34	10.33	0.00	0.00	0.00
	3	196.41	1637.82	1.15	0.00	0.00	0.00
	32 S5	260.34	2844.08	17.71	0.00	0.00	0.0
	S6	260.34	2844.08	17.71	0.00	0.00	0.0
	W1	-1848.62	-5194.35	12.39	00.00	0.00	0.0
	W2	-1988.31	-3271.08	16.03	00.00	0.00	0.00
	W3	175.27	-4458.41	-1.15	0.00	0.00	0.0
	W4	45.86	-1/65.93	0.23	0.00	0.00	0.00
	9/0	783.49	-1666.58	C9'0-	0.0	0.0	0.0
	2M	53.70	4374.05	716.35	0.00	0.00	0.00
	W8	-140.39	-1718.67	184.51	0.00	0.00	0.0
	D1	-25.48	281.52	0.31	00.00	0.00	00.00
	SO	-289.76	2721.03	1.13	0.00	0.00	0.0
	SI	-237.63	2806.44	3.23	0.00	0.00	0.0
	52	-237.63	2806.44	3.23	0.00	0.00	0.0
	86	-181.23	1661.32	0.95	0.00	0.00	0.00
	W1	-549.27	-4063.38	-1.84	0.00	0.00	0.0
	W2	-392.53	-2147.01	-1.24	0.00	0.00	0.00
B4	W3	26.61	-3445.57	-1.35	0.00	0.00	0.00
	WF	1484.30	4402.57	8.84	0.00	0.0	0.0
	W6	1641.12	-2485.35	6.68	0.00	0.00	0.00
	W7	-248.28	-5148.06	653.66	00.00	0.00	0.0
	W8	-100.81	-2454.64	120.52	0.00	0.00	0.0



Node	Result Case	FX	FY	FZ	MX	Μ	MZ
		q	q	q	lb-in	lb-in	lb-in
11	D1	0.07	12.15	0.24	0.00	0.00	0.00
41	SO	17.82	305.08	1.46	00.00	00.0	00.00
11	S1	50.18	239.88	1.32	00.00	00.00	00.00
41	S2	50.18	239.88	1.32	00.0	0.00	00.00
41	S5	-33.09	278.38	1.29	00.00	00.0	00.00
11	S6	-33.09	278.38	1.29	00.00	00.00	00.00
41	W1	-666.43	-1309.80	-55.43	00.00	00.0	0.00
41	W2	-811.21	-983.88	-29.87	00.0	0.00	0.00
41	W3	671.56	-422.59	-514.15	00.00	00.0	0.00
11	W4	494.31	-861.12	-1214.03	00.0	0.00	0.00
11	W5	519.72	-31.43	-69.84	00.00	00.00	0.00
A1	W6	374.92	294.53	-41.97	00.0	0.00	00.00
11	W7	-69.94	-289.64	206.96	00.00	00.00	00.00
11	W8	-182.33	-577.53	48.41	00.0	0.00	0.00
42	D1	-0.03	18.76	0.01	00.00	00.0	0.00
42	SO	2.56	686.81	0.07	00.00	00.0	0.00
42	S1	10.82	155.01	0.07	00.0	0.00	00.00
42	S2	10.82	155.01	0.07	00.00	00.00	00.00
22	R	0 20	DAD EE	0.05		000	0.00

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LIGHTWEIGHT DESIGN, INC

Vode Result Case	χ.Ξ	<u></u> ∠ 4	전 역	MX Ni-d	M Hi-d	MZ Ih-in
<u>S0</u>					0.00	
SI	255.15	2127.49	-6.99	00.0	0.00	0.00
S2	255.15	2127.49	-6.99	0.00	00.00	0.00
S5	327.74	3632.11	0.40	00.00	00.00	0.00
S6	327.74	3632.11	0.40	0.00	0.00	0.00
W1	-1957.68	-5754.26	-0.41	0.00	0.00	0.00
W2	-2125.48	-3257.51	-0.31	0.00	0.00	0.00
W3	284.49	-5833.35	-382.21	0.00	0.00	0.00
W4	118.95	-3820.29	69.8/6-	0.00	0.00	0.00
SW	003.3/ 405 76	10 00/2-	0.08	0.0	0.0	0.00
W0 W7	-232.41	16.6405-	-1.38	0.0	0.0	00.0
W8	-483.13	-2572.65	0.12	0.00	0.00	0.00
01	-27.11	301.31	-0.79	0.00	0.00	0.00
SO	-361.11	3465.18	-14.24	00.0	00.00	0.00
S1	-292.28	3584.12	0.26	00.0	00.00	00.00
S2	-292.28	3584.12	0.26	00.0	00.0	0.00
S5	-229.28	2116.19	-19.67	0.00	0.00	0.00
S6	-229.28	2116.19	-19.67	0.00	0.00	0.00
W1	-613.92	-4651.23	-0.59	0.00	0.00	0.00
W2	-417.78	-2182.55	-2.34	0.00	0.00	0.00
W3	-100.11	-4666.79	-288.42	0.00	0.00	0.00
W4	190.82	1/.9//2-	-916.42	0.00	0.00	0.00
CVV	7401.57	-09.10.07	0.40	0.00	0.00	0.00
M6	19.000	-444/.U/	0.47	0.00	0.00	0.00
VV/ VV/O	101001	LT'CTOC-	CT'0-	00.0	0.0	0.0
M0	00'TOT-	01 C1	000	00.0	00.0	00.0
2 2	64 75	446.81	-0.16	00.0	0000	0.00
8 27	71.19	322.78	62.0-	00.0	0.00	0.0
22	71.19	322.78	-0.29	00.00	0.00	0.00
SS	-38.17	435.55	0.01	00.0	00.00	00.00
S6	-38.17	435.55	0.01	00.0	00.00	00.00
W1	-720.76	-1487.75	72.26	0.00	0.00	0.00
W2	-961.08	-1034.29	49.81	0.00	0.00	0.00
M3	835.79	221.33	1.15	0.00	0.00	0.00
W4	546.87	1006.09	3.61	0.00	0.00	0.00
CW 2011	21.424	110.01	24.60	00.0	0.00	00.0
WO W7	97.967	-2721 43	10.4 10.088	0.0	0.00	0.00
WB	-366.68	-1703.38	247.46	00.0	0.00	0.00
D1	0.04	23.21	0.01	00.0	0.00	0.00
SO	5.18	1094.66	0.03	0.00	0.00	0.00
S1	15.38	239.69	0.03	0.00	0.00	0.00
S2	15.38	239.69	0.03	0.00	0.00	0.00
ያ ያ	87.01-	1500.96	0.01	0.00	0.00	0.00
M1	-104.81	-1230.30	60.0-	0.0	0.0	0.00
WZ	66'66-	-522.71	-0.06	00.00	0.00	0.00
W3	87.76	-2688.86	-0.57	00.0	00.0	0.00
W4	81.26	-1821.79	-1.54	0.00	0.00	0.00
W5	97.82	-2683.21	-0.07	0.00	0.00	0.00
000	0/.201	0/10/61-	-0.03	00.0	0.00	00.0
V/V V/K	-124.02	144.30	1.03	00.0	0.0	0.0
01	0.15	30 51	1770	0.0	0.0	0.0
20	6.33	1318.41	0.01	0.00	0.00	0.00
S1	14.10	1790.87	0.01	00.0	00.00	00.00
S2	14.10	1790.87	0.01	00.00	00.00	00.0
S5	-3.60	478.33	0.00	0.00	0.00	0.00
S6	-3.60	478.33	0.00	0.00	0.00	0.00
LW	-90.45	-2090.48	0.00	0.00	0.00	0.00
W3	72.65	-728.70	0.02	0.00	0.00	0.00
W4	68.97	172.56	0.09	00.0	0.00	0.00
\\\L	100	10 0020		0000		

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INOUE	Result Case	EX	F	FZ	×Ψ	M	MZ
		ql	q	q	lb-in	lb-in	lb-in
03	W6	87.33	-1949.70	-0.04	0.00	00.00	0.00
03	W7	-123.91	-3798.28	-0.13	0.00	0.00	0.00
03	W8	-111.90	-2847.38	-0.04	00.00	00.00	0.00
4	D1	-1.45	19.91	0.01	0.00	00.00	0.00
4	SO	-94.56	855.57	-0.31	00.00	00.00	0.00
4	S1	-63.55	720.41	-0.20	0.00	00.00	0.00
4	S2	-63.55	720.41	-0.20	0.00	0.00	0.00
4	S5	-46.40	625.81	-0.23	00.00	00.00	0.00
4	S6	-46.40	625.81	-0.23	0.00	00.00	0.00
4	W1	-635.41	-938.40	35.26	0.00	0.00	0.00
4	W2	-431.39	-222.81	7.64	0.00	00.00	0.00
4	W3	-72.02	-1451.36	0.82	00.00	00.00	0.00
4	W4	103.04	-226.09	1.15	0.00	00.00	0.00
4	W5	1111.09	-2324.31	84.49	00.00	00.00	0.00
4	W6	1315.35	-1610.38	57.37	00.00	00.00	0.00
4	W7	-655.62	-2004.35	790.54	00.00	00.00	00.00
4	W8	-422.67	-860.13	161.74	0.00	00.00	0.00

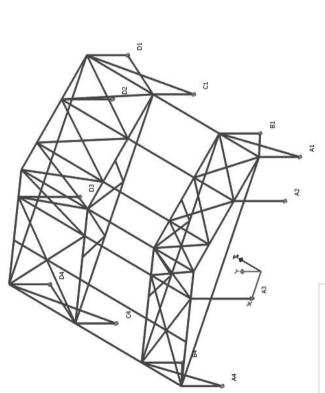
Approved for Construction TSTR-20-01723 11/03/20

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LIGHTWEIGHT DESIGN, INC

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D1 - Dead Load
W1/W5- Wind, +X/-X with over-pressure
W2/W6- Wind, +X/-X with under-pressure
W3/W7- Wind, +Z/-Z with over-pressure
W4/W8- Wind, +Z/-Z with under-pressure
S0- Balanced Snow Load
S1,S2,S3,S4,S5,S6,S7,S8- Unbalanced Snow Load

17.01 89.06 89.06 89.06 89.06 85.39.49 673.36 673.36 673.36 475.26 477.06 477.06 608.64 477.06 608.64 112.90.00 964.04

0.10 0.10 3.35.68 3.35.68 2.30.66 2.31.53 2.30.66 2.217.53 2.217.5

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MZ lb-in

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Node Re	Node Reactions-Complined Loads						
Node	Result Case	Щ.	2 4	E7 d	XX ri-d	M ∀ ri-d	MZ di-di
	6.03-0.9D1+1.0W3	668.52	-410.86	-511.21	0.00	0.00	0.00
A1	6.04-0.9D1+1.0W4		-851.05	-1211.20	0.00	0.00	0.00
	6.05-0.9D1+1.0W5	519.90	-11.59	-66.05	0.00	0.00	0.00
A1	6.06-0.9D1+1.0W6	375.09	315.97	-37.01	0.00	0.00	0.00
	6.07-0.9D1+1.0W7	-66.26	-265.53	207.18	0.00	0.00	0.00
A1	6.08-0.9D1+1.0W8	-178.83	-553.31	48.57	0.00	0.00	0.00
A2	1.01-1.4D1	-0.05	26.27	0.02	0.00	0.00	0.00
¥2	TMC:0+0C0:T+TC/Z:T-ZT:C	10.65-	01 777	0.00	0.00	0.00	00.0
44	2 14-1 2D1+1.020+0.5M2	73.75	77.75	-106.70	0.00	0.00	0.00
A7	3 15-1 2D1+1 6S0+0 5W4	36.41	171 18	-518 24	0.00	0.00	0.00
A2	3.16-1.2D1+1.6S0+0.5W5	34.95	405.97	0.07	0.00	0.00	0.00
R2	3.17-1.2D1+1.6S0+0.5W6	35.99	628.72	0.09	0.00	0.00	0.00
A2	3.18-1.2D1+1.6S0+0.5W7	-23.73	1067.83	420.48	00.0	0.00	00.0
A2	3.19-1.2D1+1.6S0+0.5W8	-22.14	1251.52	98.53	00.0	0.00	0.00
A2	3.21-1.2D1+1.6S1+0.5W1	-18.40	-370.10	0.07	0.00	0.00	0.00
FZ :	3.22-1.2D1+1.6S2+0.5W2	-20.91	-114.89	60.0	0.00	0.00	0.00
¥ ç	3.25-1.2U1+1.053+U.5W3	44.04	-1000 27	-190.80	0.00	0.00	0.00
A2	3.25-1.2D1+1.655+0.5W5	6.72	884.46	0.05	0.00	0.00	0.00
A2	3.26-1.2D1+1.6S6+0.5W6	14.52	1070.42	0.07	0.00	0.00	0.00
A2	3.27-1.2D1+1.6S7+0.5W7	-38.44	58.43	420.31	0.00	0.00	0.00
A2	9	-33.44	221.38	98.42	0.00	0.00	0.00
A2	6.01-0.9D1+1.0W1	-88.55	-1115.42	-0.08	0.00	0.00	0.00
A2	6.02-0.9D1+1.0W2	-85.90	-670.97	-0.04	0.00	0.00	0.00
A C	6.03-0.9D1+1.0W3	89.32	-2543.06	-393./3	0.00	0.00	0.00
AZ C	6.04-0.9D1+1.0W4	84.72	-20.86.02	C0.02-10.50.0	0.00	0.00	0.00
42 47	5.05-0.0014110005	63.33	-063 05	10.0-	0.00	000	0.00
24	6 07-0 9D1+1 0W7	-78.21	10.00	840.61	000	0000	0000
A2	6.08-0.9D1+1.0W8	-68.18	425.34	196.83	0.00	0.00	0.00
A3	1.01-1.4D1	0.18	38.39	0.00	0.00	0.00	0.00
A3	3.12-1.2D1+1.6S0+0.5W1	-31.77	514.95	0.02	00.0	0.00	00.0
A3	3.13-1.2D1+1.6S0+0.5W2	-30.58	782.03	0.03	0.00	0.00	00.0
A3	3.14-1.2D1+1.6S0+0.5W3	31.41	994.09	-302.90	0.00	0.00	0.00
A C	3.15-1.2D1+1.6S0+0.5W4	32.05	1224.16	/5./6/-	0.00	0.00	0.00
A3 A3	3.17-1.2D1+1.05U+U.5W5	31.08	809.38 1076 44	0.00	0.00	0.00	0.00
A3	3 18-1 2D1+1 6S0+0 5W7	-16.41	686.70	646.83	000	000	0.00
R R	3.19-1.2D1+1.6S0+0.5W8	-15.58	882.57	151.47	0.00	0.00	0.00
A3	3.21-1.2D1+1.6S1+0.5W1	-14.57	1038.48	0.02	0.00	0.00	0.00
A3	3.22-1.2D1+1.6S2+0.5W2	-16.41	1282.70	0.03	0.00	0.00	0.00
A3	3.23-1.2D1+1.6S3+0.5W3	36.03	-283.70	-302.93	0.00	0.00	0.00
A V	3.24-1.2U1+1.654+0.5W4	34.1/	-62.11	10.04	0.00	0.00	0.00
A3	3.26-1.2D1+1.656+0.5W6	17.74	211.26	0.00	0.00	0.00	0.00
A3	3.27-1.2D1+1.6S7+0.5W7	-31.84	-747.75	646.75	0.00	0.00	0.00
A3	3.28-1.2D1+1.6S8+0.5W8	-27.85	-507.93	151.45	0.00	0.00	0.00
A A	6.01-0.9D1+1.0W1	80.//- 2C.VC	-1/38.93	-0.02	0.00	0.00	0.00
22	0.02-0.301+1.0WZ	00 62	70'06TT-	-605.87	0.00	0000	0000
2 2	6.04-0.9D1+1.0W4	69.20	-158.38	-1595.14	0.00	0.00	0.00
Ra Ra	6.05-0.9D1+1.0W5	50.39	-1144.81	-0.07	0.00	0.00	0.00
A3	6.06-0.9D1+1.0W6	53.21	-600.94	-0.05	0.00	0.00	0.00
A3	6.07-0.9D1+1.0W7	-65.08	-1549.04	1293.49	0.00	0.00	0.00
	6.08-0.9D1+1.0W8	-57.05	-1067.24	302.88	0.00	0.00	0.00
	1.01-1.4D1	-0.84	24.12	0.35	0.00	0.00	0.00
	2.12-1.2D1+1.650+U.5WI	07,000-	PD:010	61.1	0.00	0.00	0.00
	3.14-1.2D1+1.6S0+0.5W2	-94.13	48.30	-755,12	0.00	0.00	0.00
	3.15-1.2D1+1.6S0+0.5W4	-36.16	-64.65	-693.92	0.00	0.00	0.00
	3.16-1.2D1+1.6S0+0.5W5	153.18	324.70	1.72	0.00	0.00	0.00
	3.17-1.2D1+1.6S0+0.5W6	213.76	541.39	2.15	0.00	0.00	0.00
A4	3.18-1.2D1+1.6S0+0.5W7	-254.05	976.17 954.20	206.20	0.00	0.00	0.00
	2.15-1.21.41.4C0.4-UC0.1+110.2.1-2.1-2.1-2.1-2.1-2.1-2.1-2.1-2.1-2.1	-195.99	357.45	50.18	0.00	0.00	0.00
	TAACOTTATOOTTATO		CL:300	104	222	200	20.0

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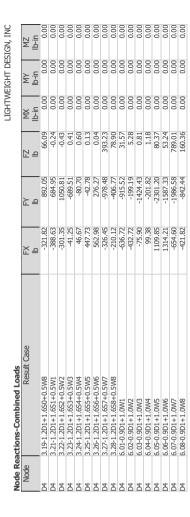
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Result Case	Т Т	<u></u> ₽	Z ₫	MX h-dl	MY h-i	MZ lb-in
3.12-1.2D1+1.6S0+0.5W1	-158.47	3061.21	0.32	0.00	0.00	0.00
3.13-1.2D1+1.6S0+0.5W2 3.14-1.2D1+1.6S0+0.5W3	-303.36 1039.93	3111.60	-200.45	0.00	0.00	0.00
3.15-1.2D1+1.6S0+0.5W4	891.13	4099.10	-503.94	0.00	0.00	0.00
3.16-1.2D1+1.6S0+0.5W5 3.17-1.2D1+1.6S0+0.5W6	1184.58	3180.59 4448.49	-5.56	0.00	0.00	0.00
3.18-1.2D1+1.6S0+0.5W7	671.54	3621.38	-0.10	0.00	0.00	0.00
3.19-1.2D1+1.6S0+0.5W8	523.91	4626.77	0.64	0.00	0.00	0.00
3.22-1.2D1+1.652+0.5W2	-610.78	7087.94	-15.4/	0.00	0.00	0.00
3.23-1.2D1+1.653+0.5W3	190.21	-2555.91	-193.24	0.00	0.00	0.00
3.24-1.2D1+1.6S4+0.5W4	107.16	-1547.54	-491.61	0.00	0.00	0.00
3.25-1.2D1+1.6S5+0.5W5	990.89	3406.91	0.74	0.00	0.00	0.00
3.26-1.2D1+1.656+0.5W6 3.27-1.2D1+1.657+0.5M7	870.60	4658.50 -1897 28	-0.58	0.00	0.00	0.00
3.28-1.2D1+1.6S8+0.5W8	-203.06	-933.95	0.11	0.00	0.00	0.00
6.01-0.9D1+1.0W1	-1922.49	-5488.13	-0.35	0.00	0.00	0.00
6.02-0.9D1+1.0VVZ 6.03-0.9D1+1.0VVZ	77.0602- 85.0C5	-5562 51	c2.0- 28.3.84	0.00	0.00	0.00
6.04-0.9D1+1.0W4	154.75	-3548.22	-980.40	0.00	0.00	0.00
6.05-0.9D1+1.0W5	698.48	-5280.00	-0.69	0.00	0.00	0.00
6.06-0.9D1+1.0W6	530.23	-2785.33	-3.00	0.00	0.00	0.00
6.0/-0.9D1+1.0W/ 6.08-0.9D1+1.0W/8	-203./b	-4234.06	-1.29	0.00	0.00	0.00
1.01-1.4D1	-37.95	421.83	-1.10	0.00	0.00	0.00
3.12-1.2D1+1.6S0+0.5W1	-1065.17	3553.94	-29.23	0.00	0.00	0.00
3.13-1.2D1+1.6S0+0.5W2	-902.70	4801.85	-34.09	0.00	0.00	0.00
3.14+1.2D1+1.6S0+0.5W3	-/31.23	3488.04	-197.09	0.00	0.00	0.00
3.16-1.2D1+1.650+0.5W5	421.18	2422.34	2.48	0.00	0.00	0.00
3.17-1.2D1+1.6S0+0.5W6	583.70	3670.17	-2.44	00.0	0.00	0.00
3.18-1.2D1+1.6S0+0.5W7	-1028.12	3054.65	0.63	0.00	0.00	0.00
3.21-1.2D1+1.6S1+0.5W3	-91112 -01112	3772.85	0.23	0.00	0.00	0.00
3.22-1.2D1+1.6S2+0.5W2	-772.02	5008.48	-3.39	0.00	0.00	0.00
3.23-1.2D1+1.6S3+0.5W3	-86.62	-1984.37	-149.98	0.00	0.00	0.00
3.24-1.2D1+1.654+0.5W4 3.25-1.2D1±1.6S5±0.5M5	28.00	-1035.33	-462.19	0.00	0.00	0.00
3.26-1.2D1+1.656+0.5W6	888.90	1474.14	-26.08	0.00	0.00	0.00
3.27-1.2D1+1.6S7+0.5W7	-196.37	-2547.78	0.01	0.00	0.00	0.00
3.28-1.2D1+1.658+0.5W8	-96.91	-1557.93	0.08	0.00	0.00	0.00
6.01-0.9D1+1.0VV1	453 35	-1017 44	-4.73	0.00	0.00	0.00
6.03-0.9D1+1.0W3	-127.66	-4404.59	-292.76	0.00	0.00	0.00
6.04-0.9D1+1.0W4	162.79	-2511.89	-919.42	0.00	0.00	0.00
6.05-0.9D1+1.0W5 6.06-0.9D1+1.0W6	2366.89	-4181 01	0.46	0.00	0.00	0.00
6.07-0.9D1+1.0W7	-334.54	-5545.30	-0.09	0.00	0.00	0.00
6.08-0.9D1+1.0W8	-135.71	-3566.46	0.06	0.00	0.00	0.00
1.01-1.4D1	0.60	16.99	0.01	0.00	0.00	0.00
3.12-1.2D1+1.6S0+0.5W1 3.13-1.2D1+1.6S0+0.5W2	-420.08	43.98	-0.21	0.00	0.00	0.00
3.14-1.2D1+1.6S0+0.5W3	408.16	715.90	0.43	0.00	0.00	0.00
3.15-1.2D1+1.6S0+0.5W4	284.61	1153.82	1.66	0.00	0.00	0.00
3.16-1.2D1+1.6S0+0.5W5	556.79	750.00	0.00	0.00	0.00	0.00
3 18-1 2D1+1 650+0 5W7	52.09	408.26	405.55	0.00	0.00	0.00
3.19-1.2D1+1.6S0+0.5W8	-70.69	33.97	90.57	0.00	0.00	0.00
3.21-1.2D1+1.6S1+0.5W1	-201.06	-70.78	-0.38	00.00	0.00	0.00
3.22-1.2D1+1.652+0.5W2	-341.50	91.59	-0.40	0.00	0.00	0.00
5.25-1.2D1+1.653+0.5W3 3.24-1.2D1+1.654+0.5W4	769.60	510.34	1.82	0.00	0.00	0.00
3.25-1.2D1+1.6S5+0.5W5	395.95	627.86	0.39	0.00	0.00	0.00
3.26-1.2D1+1.6S6+0.5W6	293.82	877.60	0.51	0.00	0.00	0.00
3.2/-1.2U1+1.65/+U.5W/	-//9/-	-1330.35	440.94	0.00	0.00	0.00

LIGHTWEIGHT DESIGN, INC

	10 10	Kesult Case	Ě	2	77	×Ψ	μ	MΖ
6.61-00+1.0.M1         5.0.03         -0.17.3         5.0.0         0.00         0.00           6.61-00+1.1.0.M3         6.61-00+1.1.0.M3         5.0.0         1.1.1.7         3.1.1.9         1.1.1	01 01		q	qI	q	lb-in	lb-in	lb-in
Condition         Condition <thcondition< th=""> <thcondition< th=""> <thc< td=""><td>D1 D1</td><td>6.01-0.9D1+1.0W1</td><td>-720.25</td><td>-1471.40</td><td>68.23</td><td>00.00</td><td></td><td>0.00</td></thc<></thcondition<></thcondition<>	D1 D1	6.01-0.9D1+1.0W1	-720.25	-1471.40	68.23	00.00		0.00
Condition (Condition)         50.35         71.35         71.37<	DI	6.02-0.9D1+1.0W2	-960.59	-1017.97	45.79	0.00	0.00	0.00
Methodont Link         Methodott         Methodottt         Me	2	6.03-0.9D1+1.0W3	832.66	227.58	1.17	0.00	0.00	0.00
Constrained (Constrained (Constrained)         Constraine (Constrained)         Constraine (Constrained)         Constraine (Constrained)         Constrained (Constrained)	14	6.05-0.9D1+1.0VV4	743.97	14.1101	5.03	0.0	0.0	0.00
Condition         Size	32		750 07	CC'/T-	14.12	0.0	0.0	0.0
111.121+103+1650-05M         362.3         156.46         364.75         0.00         0.00           111.121+1153+1650-05M         111.123+11650-05M         364.75         0.00         0.00         0.00           111.121+1153+1650-05M         37.81         37.81         37.81         0.01         0.00         0.00           111.121+1153+1650-05M         38.16         37.44         0.05         0.00         0.00         0.00           111.121+1153+1650-05M         38.16         37.44         0.05         0.00         0.00         0.00           111.121+1153+1650-05M         38.16         37.45         0.05         0.00         0.00         0.00           111.121+1153+1650-05M         38.16         37.45         0.05         0.00         0.00         0.00           121.121+1650-05M         38.16         17.46         10.75         0.01         0.00         0.00           121.121+1650-05M         38.14         17.75         0.12         0.02         0.00         0.00         0.00           121.121+1650-05M         38.14         17.75         0.01         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00	3 2	0.00-0.501±1.0000	120.021	201/07	0.00	0.0	0.0	0.0
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	52	6.08-0 9D1+1 0W8	C 292-	-1681 45	244.47	0000	0.0	0.00
111.1.201+1680-6 MG         114.73         0.00         0.00           111.1.201+1680-6 MG         9.94         9.74         9.06         0.00         0.00           111.1.201+1680-6 MG         9.94         9.34         9.04         0.00         0.00           111.1.201+1680-6 MG         9.94         9.34         9.04         0.00         0.00           111.1.201+1680-6 MG         9.94         9.34         0.00         0.00         0.00           111.1.201+1680-6 MG         9.94         9.34         0.00         0.00         0.00           221.1.201+1680-6 MG         9.94         1.9475         0.01         0.00         0.00           221.1.201+1680-6 MG         9.94         9.34         1.9475         0.01         0.00         0.00           221.1.201+1680-6 MG         9.94         1.9435         0.13         0.00         0.00         0.00           221.1.201+1680-6 MG         9.94         1.9435         0.13         0.00         0.00         0.00           221.1.201+1680-6 MG         9.94         1.9435         0.13         0.00         0.00         0.00           221.1.201+1680-6 MG         9.94         1.9435         0.01         0.00         0.00	5	1 01-1 401	0.06	32.50	0.01	000	00.0	0.00
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	32	12-1 2D1±1 6S0±0	41 03	1147 37	10.0	0000	0.0	000
111:1.121:1.1201:1.12	20		08 02	1502 78	20.0	0.0	0.0	0.0
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	22		20'00- L0 L0	07'COLT	70.0	0.0	0.0	0.0
Jist. Dist. Dist. Sector         Sist.         Sus.	70	5.17-1.2D1+1.050+1.5C0+0.2015	20.02	CU.2/C	07.0-	00.00	0.00	00.0
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	70	3.15-1.2D1+1.6S0+0.5W4	39.44	960.84	0.74	0.00	0.00	0.00
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	70	3.16-1.2D1+1.0S0+0.5V0+0.2VV5	58.16	431.42	0.04	0.00	0.00	0.00
31911201+1659-05W         6674         139436         0.09         0.00         0.00           31911201+1659-05W         1491201+1659-05W         1491201         0.01         0.00         0.00           31911201+1659-05W         3241201+1659-05W         14973         0.11         0.00         0.00         0.00         0.00           32511201+1656-05W         14973         0.13         0.01         0.00	D2	3.17-1.2D1+1.6S0+0.5W6	60.18	787.40	0.05	0.00	0.00	0.00
31911201+1659-0500         31911201+1659-0500         0.01         0.00         0.00           32511201+1655-0500         32511201+1655-0500         0.03         0.00         0.00         0.00           32511201+1655-0500         32511201+1655-0500         0.03         0.00         0.00         0.00           32511201+1655-0500         3250         1232120         0.03         0.00         0.00         0.00           32511201+1655-0500         3250         1232120         0.03         0.00         0.0	D2	3.18-1.2D1+1.6S0+0.5W7	-46.74	1534.66	0.69	00.0	0.00	0.00
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	D2	3.19-1.2D1+1.6S0+0.5W8	-44.94	1907.73	0.17	00.0	0.00	0.00
3.2.3.1.2.01:H.655-0.502         0.04         0.04         0.00         0	D2	3.21-1.2D1+1.6S1+0.5W1	-17.50	-294.92	0.03	0.00	0.00	0.00
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	D2	3.22-1.2D1+1.6S2+0.5W2	-19.69	99.89	0.04	00.0	0.00	0.00
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	D2	3.23-1.2D1+1.6S3+0.5W3	42.80	-1304.95	-0.28	00.0	0.00	00.00
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	D2	3.24-1.2D1+1.6S4+0.5W4	39.68	-872.71	-0.77	00.00	0.00	0.00
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	D2	3.25-1.2D1+1.6S5+0.5W5	22.59	1183.92	0.01	00.00	0.00	0.00
3.27.120+1165+0.5W         -72.50         5.7.34         0.05         0.00         0.00           601.9091+1.0W1         58.97         -26.96         -7.34         0.15         0.00         0.00           601.9091+1.0W1         60.9091+1.0W1         10.475         -7.734         0.15         0.00         0.00           601.9091+1.0W1         60.9091+1.0W1         85.97         -266.52         0.06         0.00         0.00           605.9091+1.0W4         85.97         -266.52         0.06         0.00         0.00           605.9091+1.0W5         619.901+1.0W5         115.23         -115.31         1.00         0.00         0.00           605.9091+1.0W5         55.91         -15.33         -15.31         1.00         0.00         0.00           607.9091+1.0W5         55.91         -15.33         -15.31         1.00         0.00         0.00           101.1401         55.91         -15.33         -15.31         1.00         0.00         0.00         0.00           31.41.1201+165.91         57.91         0.01         0.00         0.00         0.00         0.00         0.00           31.41.1201+165.91         57.91         57.91         0.01         0.00 <td< td=""><td>D2</td><td>3.26-1.2D1+1.6S6+0.5W6</td><td>29.14</td><td>1497.01</td><td>0.02</td><td>00.00</td><td>0.00</td><td>0.00</td></td<>	D2	3.26-1.2D1+1.6S6+0.5W6	29.14	1497.01	0.02	00.00	0.00	0.00
3.9.1.20+1.168.0.5%6 $6.601$ $2.77.64$ $0.12$ $0.00$ $0.00$ $6.01.9.0.9.1+1.0N1$ $6.8.97$ $-3.57.64$ $0.12$ $0.00$ $0.00$ $6.02.9.091+1.0N1$ $6.8.97$ $-3.53.94$ $0.05$ $0.00$ $0.00$ $6.07.9091+1.0N1$ $6.8.97$ $-3.53.94$ $0.05$ $0.00$ $0.00$ $6.07.9091+1.0N3$ $6.8.97$ $-3.53.94$ $-3.53.94$ $-0.56$ $0.00$ $0.00$ $6.07.9091+1.0N4$ $8.8.97$ $-3.53.3$ $-13.33$ $-13.33$ $0.00$ $0.00$ $6.07.9091+1.0N4$ $0.01.1.01.012$ $0.02.20.000$ $0.00$ $0.00$ $0.00$ $10.1+01$ $3.15-1.21+1.65.40.5M1$ $-3.32.31.13.13.13.13.13.13.13.13.13.13.13.13.$	D2	3.27-1.2D1+1.6S7+0.5W7	-72.50	-53.28	0.55	00.00	0.00	0.00
607-0091+10W1         -104.75         -1202-38         -0.08         0.00         0.00           607-0091+10W4         607-0091+10W4         85.97         -56.95         -6.75         0.07         0.00         0.00           607-0091+10W4         607-0091+10W4         97.94         -76.92         0.00         0.00         0.00           607-0991+10W4         97.94         -76.72         0.00         0.00         0.00         0.00           607-0991+10W6         -15.33         -13.23         -51.13         1.02         0.00         0.00         0.00           608-0991+10W6         -15.32         -13.23         -51.13         1.15.25         0.00         0.00         0.00           13.12-120+1650+05W1         -33.18         111.52         0.02         0.00         0.00         0.00           3.15-120+1650+05W1         -33.18         111.52         0.02         0.00         0.00         0.00           3.15-120+1650+05W1         -33.18         117.35         0.01         0.00         0.00         0.00           3.15-120+1650+05W1         -31.23         173.36         0.01         0.00         0.00         0.00           3.15-120+1650+05W1         -31.23         173.36	D2	3.28-1.2D1+1.6S8+0.5W8	-66.01	277.64	0.12	00.0	00.0	0.00
602.9091+10W2 $603.901+10W2$ $60.901+10W3$ $10.330$ $10.331$ $10.331$ $10.301$ $10.90$ $0001$ <t< td=""><td>D2</td><td>6.01-0.9D1+1.0W1</td><td>-104.75</td><td>-1209.28</td><td>-0.08</td><td>0.00</td><td>0.00</td><td>00.0</td></t<>	D2	6.01-0.9D1+1.0W1	-104.75	-1209.28	-0.08	0.00	0.00	00.0
6(3,9,0)1+1,0M3 $66,9'$ $-56,5,96$ $0,5'$ $0,00$	D2	6.02-0.9D1+1.0W2	-99.93	-501.66	-0.05	00.00	0.00	00.00
604-590+1.0W1 $605-390+1.0W1$ $605-390+1.0W1$ $1.53$ $0.00$ $0.$	D2	6.03-0.9D1+1.0W3	86.97	-2659.64	-0.57	0.00	0.00	0.00
666-0301+1.0NG         566.2.2         0.06         0.00         0.00           666-0301+1.0NG         1.12.80         -59.4.75         0.02         0.00         0.00           607-0301+1.0NG         1.13.23         53.1.18         0.22         0.00         0.00         0.00           1.011-1401         1.115.22         53.1.18         0.02         0.00         0.00         0.00           1.011-1401         -3.1.12         1.13.22         53.1.18         0.02         0.00         0.00         0.00           3.12-1.211+1550-0.5NN2         -3.1.23         3.1.1.212         1.13.26         0.01         0.00         0.00         0.00           3.14-1.211+1550-0.5NN2         3.14         1.13.56         0.01         0.00         0.00         0.00         0.00           3.14-1.211+1550-0.5NN2         3.14         1.13.56         0.01         0.00         0.01 <td>D2</td> <td>6.04-0.9D1+1.0W4</td> <td>80.54</td> <td>-1793.14</td> <td>-1.53</td> <td>00.00</td> <td>0.00</td> <td>0.00</td>	D2	6.04-0.9D1+1.0W4	80.54	-1793.14	-1.53	00.00	0.00	0.00
666-3901+1.007 $100.280$ $1954.75$ $0.02$ $0.00$	D2	6.05-0.9D1+1.0W5	97.90	-2662.22	-0.06	0.00	0.00	0.00
607-050111001         116.33         130.31         110         0.00	20	6.06-0 9D1+1 0W6	102.02	-1954 75	0.0	000	00.0	0.00
600000         0000000         00000000         000000000000000000000000000000000000	30	6.07-0.9D1+1.0W7	-146.33	-130.31	1 09	000	00.0	0.00
101-1401         0.20         4.2.71         0.00         0.00         0.00           313-12.20+16590-5W1         313-131.09         0.02         0.00	20	6.08-0.9D1+1.0W8	-133.29	531.18	0.22	0.00	0.00	0.00
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	5	1.01-1.4D1	0.0	42.71	00.0	00.0	00.0	0.00
3.13-1.D1+1.630+0.5W2 $3.12.2$ $1531.09$ $0.02$ $0.00$ </td <td>200</td> <td>3 12-1 2D1+1 6S0+0 5W1</td> <td>-33.18</td> <td>1115.22</td> <td>0.00</td> <td>000</td> <td>00.0</td> <td>0.00</td>	200	3 12-1 2D1+1 6S0+0 5W1	-33.18	1115.22	0.00	000	00.0	0.00
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	200	3 1 3-1 2D1+1 6S0+0 5W2	-31 22	1531.09	0.02	000	00.0	0.00
315-1.D1+1.630+0.5Wit $5.810$ $2183.96$ $0.03$ $0.00$ <td>32</td> <td>3 14-1 2D1+1 6S0+0 5W3</td> <td>34 54</td> <td>1713.05</td> <td>0.03</td> <td>0000</td> <td>00.0</td> <td>000</td>	32	3 14-1 2D1+1 6S0+0 5W3	34 54	1713.05	0.03	0000	00.0	000
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	D3	3.15-1.2D1+1.6S0+0.5W4	36.80	2188.98	0.03	0.00	0.00	0.00
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	200	3.16-1.2D1+1.6S0+0.5W5	57.37	758.04	0.0	000	00.0	0.00
318-1201+1636-0.5W7         -36.30         -337.75         0.00         0.00         0.00           319-1201+1656-0.5W8         -34.23         785.76         0.01         0.00         0.00         0.00           327-1201+1657-0.5W2         -34.23         785.76         0.01         0.00         0.00         0.00           327-1201+1657-0.5W2         -15.94         230.941         0.01         0.00         0.00         0.00           327-1201+1657-0.5W2         -15.94         230.941         0.01         0.00         0.00         0.00           327-1201+1657-0.5W3         33.44         119.82         0.01         0.00         0.00         0.00           327-1201+1658-0.5W5         33.44         119.82         0.01         0.00         0.00         0.00           327-1201+1658-0.5W5         33.44         119.82         0.01         0.00         0.00         0.00           327-1201+1658-0.5W5         33.14         -60.54         0.01         0.00         0.00         0.00           327-1201+1658-0.5W5         33.14         -135.65         0.01         0.00         0.00         0.00           327-1201+1658-0.5W5         33.14         -135.65         0.01         0.00         <	5	3.17-1.2D1+1.6S0+0.5W6	54.31	1173.85	-0.01	0.00	0.00	0.00
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	D3	3.18-1.2D1+1.6S0+0.5W7	-36.30	337.75	00.0	0.00	0.00	0.00
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	5	3.19-1.2D1+1.6S0+0.5W8	-34.73	785.76	0.0	000	00.0	0.00
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	2 C	3.21-1.2D1+1.6S1+0.5W1	-13.85	1917.57	0.01	00.0	0.00	0.00
3.2.3-1.2D1+1.653+0.5M3     35.56     -330.55     0.01     0.00     0.00       3.2.5-1.2D1+1.655+0.5W4     3.3.4     13.3.4     13.3.4     13.0.6     0.01     0.00     0.00       3.2.5-1.2D1+1.655+0.5W6     3.3.4     -300.61     0.01     0.00     0.00       3.2.5-1.2D1+1.655+0.5W6     3.3.14     -306.61     0.01     0.00     0.00       3.2.5-1.2D1+1.655+0.5W6     5.4.98     1381.35     0.01     0.00     0.00       3.2.7-1.2D1+1.655+0.5W6     5.4.98     1381.35     0.02     0.00     0.00       3.2.7-1.2D1+1.658+0.5W6     5.4.98     1381.35     0.02     0.00     0.00       5.2.7.1.2D1+1.658+0.5W6     5.4.98     1381.35     0.01     0.00     0.00       6.00-0.9D1+1.0W1     5.8.48     1381.35     0.02     0.00     0.00       6.07-0.9D1+1.0W1     5.8.48     137.51     192.03     0.00     0.00       6.05-0.9D1+1.0W1     5.8.48     1381.35     0.02     0.00     0.00	ED	3.22-1.2D1+1.6S2+0.5W2	-15.49	2309.41	0.01	00.0	0.00	0.00
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	D3	3.23-1.2D1+1.6S3+0.5W3	35.56	-330.95	0.01	00.0	0.00	00.00
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	D3	3.24-1.2D1+1.6S4+0.5W4	33.84	119.82	0.04	0.00	0.00	0.00
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	D3	3.25-1.2D1+1.6S5+0.5W5	27.40	-637.79	-0.01	00.00	0.00	00.0
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	D3	3.26-1.2D1+1.6S6+0.5W6	33.14	-200.61	-0.01	00.00	00.00	00.00
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	B	3.27-1.2D1+1.6S7+0.5W7	-60.94	-1856.59	-0.06	0.00	0.00	0.00
6.02-0901+1.0W1         -90.31         -2052.47         0.00	ñ	3.28-1.2D1+1.6S8+0.5W8	-54.98	-1381.35	-0.02	0.00	0.00	0.00
6.03-091+1.0W3         -0.03         0.00         0.00         0.00         0.00           6.03-091+1.0W4         6.03-091+1.0W4         6.03         0.01         0.00         0.00         0.00           6.04-091+1.0W4         6.03-091+1.0W4         8.48         197.61         0.09         0.00         0.00         0.00           6.05-091+1.0W5         8.48         197.61         0.09         0.00         0.00         0.00           6.05-091+1.0W5         8.731         -192.0.8         0.01         0.00         0.00         0.00           6.05-091+1.0W5         8.731         -192.0.8         0.01         0.00         0.00         0.00           6.05-091+1.0W5         8.731         -192.0.8         0.01         0.00         0.00         0.00           6.06-091+1.0W5         8.731         -192.0.8         0.13         0.00         0.00         0.00           10.11-01         -11.1-01         -12.31.5         -37.65         0.01         0.00         0.00           3.13-1.201+1.6080-5W1         -23.52         0.01         0.00         0.00         0.00           3.13-1.201+1.6500-5W1         -37.85         0.01         0.00         0.00         0.00         0.00 </td <td>20</td> <td>6.01-0.9D1+1.0W1</td> <td>-90.31</td> <td>-2062.47</td> <td>0.00</td> <td>0.00</td> <td>0.00</td> <td>0.00</td>	20	6.01-0.9D1+1.0W1	-90.31	-2062.47	0.00	0.00	0.00	0.00
604-0.901+1.0W5         97.131-1.911         235.55         97.131-1.91 </td <td>3 2</td> <td>ZM0.1+100.0-20.0</td> <td>00.00-</td> <td>+0.521-</td> <td>10.0</td> <td>0.0</td> <td>0.0</td> <td>00.0</td>	3 2	ZM0.1+100.0-20.0	00.00-	+0.521-	10.0	0.0	0.0	00.0
6.05-0.901+1.0W5         8.214         2.752.04         0.03         0.00	3 2		60.21	107.01	0.02	000	00.0	0.0
6.66 - 0.901+1.000         87.51         1-920.82         0.04         0.00         0.00           6.07 - 0.901+1.000         6.07 - 0.901+1.000         5.07         9.091+1.000         0.00         0.00         0.00           6.06 - 0.901+1.000         6.07 - 0.901+1.000         2.011         2.315.55         -0.13         0.00         0.00           6.08 - 0.901+1.000         2.011         2.215.55         -0.13         0.00         0.00           1.01-1.4D1         2.215.11         -225.50         2.787         0.01         0.00         0.00           3.13-1.201+1.6590-5001         -365.57         1-904.22         0.46         0.00         0.00           3.13-1.201+1.6590-5003         3.13-1.201+1.6590-5003         -365.57         1-904.22         0.010         0.00           3.13-1.201+1.6590-5004         -365.57         1-904.22         0.510         0.00         0.00           3.13-1.201+1.6590-5004         -355.60         757.64         0.10         0.00         0.00           3.14-1.2014-1.6590-5004         -355.60         757.64         0.10         0.00         0.00           3.15-1.201+1.6590-5004         -314.23         252.52         0.013         0.00         0.00           3.15-1.2	32	6 05-0 0D1+1 0MF	82 01	10.761	100	0000	0.0	0.00
6.0 <sup>+</sup> 0.991+1.0W7         -123.15         -7766.36         0.13         0.00         0.00           6.0 <sup>+</sup> 0.991+1.0W7         6.08-0.901+1.0W7         -111.19         -2815.56         0.13         0.00         0.00         0.00           6.0 <sup>+</sup> 0.991+1.0W8         -111.19         -2815.56         0.013         0.00         0.00         0.00           1.01-1.401         -2815.56         0.41.23         0.46         0.00         0.00         0.00           3.12-1.201+1.650+0.5W1         -464.60         94.123         0.46         0.00         0.00         0.00           3.13-1.201+1.650+0.5W2         -365.57         1290.42         0.59         0.00         0.00         0.00           3.15-1.201+1.650+0.5W4         -355.50         71290.42         0.01         0.00         0.00         0.00           3.15-1.201+1.650+0.5W6         -365.57         1290.42         0.31         0.00         0.00         0.00           3.15-1.201+1.650+0.5W6         0.165.65         0.13         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00	82	6 06-0 9D1+1 0W/6	87 51	-1920.82	60.0 40 0-	0000	0.0	000
6.08-0.9D1+1.0W8         -1111:9         -2815.56         -0.05         0.00         0.00           1.01-1.4D1         -2.04         27.87         0.01         0.00         0.00           3.12-1.2D1+1.630-0.5W1         -46.40         94.23         0.01         0.00         0.00           3.13-1.2D1+1.630-0.5W2         -363.57         1290.42         0.59         0.00         0.00           3.13-1.2D1+1.650-0.5W2         -363.57         1290.42         0.59         0.00         0.00           3.15-1.2D1+1.650-0.5W4         -131.91         1346.02         0.31         0.00         0.00           3.15-1.2D1+1.650-0.5W6         505.81         505.82         0.13         0.00         0.00           3.15-1.2D1+1.650-0.5W6         216.23         0.13         0.00         0.00         0.00           3.15-1.2D1+1.650-0.5W6         216.23         0.13         0.00         0.00         <	2 2 2	6.07-0.9D1+1.0W7	-123.15	-3766.36	-0.13	0.00	0.00	0.00
1.01-1.4D1         2.04         27.87         0.01         0.00         0.00           31.3-1.2D1+1.6S9-0.5W1	D3	6.08-0.9D1+1.0W8	-111.19	-2815.56	-0.05	00.00	00.00	0.00
3.12-1.2D1+1.6S0+0.5W1         -464.60         944.23         0.46         0.00         0.00           3.13-1.2D1+1.6S0+0.5W2         -363.57         1290.42         0.59         0.00         0.00           3.13-1.2D1+1.6S0+0.5W2         -363.57         1290.42         0.19         0.00         0.00           3.14-1.2D1+1.6S0+0.5W3         -313.91         1746.02         0.31         0.00         0.00           3.15-1.2D1+1.6S0+0.5W5         -313.91         1746.02         0.31         0.00         0.00           3.16-1.2D1+1.6S0+0.5W5         505.81         505.81         531.91         0.03         0.00         0.00           3.16-1.2D1+1.6S0+0.5W6         505.81         505.81         505.81         505.81         0.03         0.00         0.00           3.16-1.2D1+1.6S0+0.5W6         505.81         505.81         505.81         505.81         0.03         0.00         0.00	8	1.01-1.4D1	-2.04	27.87	0.01	0.00	0.00	0.00
3.13-1.2D1+1.650+0.5M2         -363.57         1290.42         0.59         0.00         0.00           3.15-1.2D1+1.650+0.5M2         -335.00         787.64         0.10         0.00         0.00           3.15-1.2D1+1.650+0.5M4         -315.11         1346.02         0.31         0.00         0.00           3.15-1.2D1+1.650+0.5M4         -131.11         1346.02         0.15         0.00         0.00           3.15-1.2D1+1.650+0.5M6         505.81         505.81         505.82         0.13         0.00         0.00           3.15-1.2D1+1.650+0.5M6         505.81         505.81         505.81         505.81         0.00         0.00           3.15-1.2D1+1.650+0.5M6         505.81         505.81         505.82         0.13         0.00         0.00	8	3.12-1.2D1+1.6S0+0.5W1	-464.60	944.23	-0.46	0.00	0.00	00.0
3.14-1.201+1.650+0.5W3         235.00         767.64         0.10         0.00         0.00           3.15-1.201+1.650+0.5W4         133.91         134.60         0.31         0.00         0.00           3.15-1.201+1.650+0.5W4         644.82         232.50         0.15         0.00         0.00           3.15-1.201+1.650+0.5W6         644.82         232.62         0.15         0.00         0.00           3.15-1.201+1.650+0.5W6         505.31         505.81         506.82         0.03         0.00         0.00           3.15-1.201+1.650+0.5W6         505.81         505.81         505.81         505.81         0.00         0.00	2	3.13-1.2D1+1.6S0+0.5W2	-363.57	1290.42	-0.59	00.0	0.00	00.0
3.15-1.2D1+1.630+0.5W4	4	3.14-1.2D1+1.6S0+0.5W3	-235.00	767.64	-0.10	00.0	00.00	0.00
3.15-1.2D1+1.639-0.5W5 40432 2.52.62 0.15 0.00 0.00 3.17-1.2D1+1.639-0.5W6 50581 59892 0.03 0.00 0.00 3.19.1 2014.1560-0.5W6 -0.00 0.00	8	3.15-1.2D1+1.6S0+0.5W4	-131.91	1346.02	0.31	0.00	0.00	0.00
0.0. 0.0. 0.0. 0.0. 0.0. 0.0. 0.0. 0.0	52		404.82	252.62	0.15	0.00	0.00	0.00
	5 2		18.505	247.92	282.64	0.00	0.0	0.0





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Member	Fx Min Ib	Fx Max Ib	≷ਵ	Mz Min Ib-in	Mz Max Ib-in
mr11	-8381.03 (25)	6991.34 (32)	-2600.16 (36)	-71006.00 (17)	523.06
mr12	-6469.85 (23)	7488.38 (32)	2563.86 (38)		124676.01 (34
mr19	-4658.50 (29)	5488.13 (32)			173569.32 (3
mr20	-10219.16 (23)	9795.83 (36)	-3321.97 (32)	-96146.60 (21)	
mr21	-/832.91 (19)	10063.15 (36)	3202.15 (34)		1/0161.43 (38
mr23	(52) 720TDC-	(95) C2.1C00	(36) 73 (36)	-199181.67 (36) -80067 05 (17)	89930.26 (J
mr74	(67) 10:76011-	(9E) TT'F /76	402) 02 (38)		170878.95 (5
mr25	-1153.82 (19)	2117.99 (38)	1330.77 (38)	-48706.38 (37)	95938.33 (5
mr26	-2211.94 (29)		-1404.25 (38)	-49010.51 (37)	96051.80 (3
mr27	-1446.89 (29)	1678.75 (34)	-1112.38 (29)	-2867.01 (37)	21800.69 (3
mr28	-1346.02 (19)		-1046.12 (34)		33612.06 (1
mr29	-2147.98 (29)		-1920.03 (36)		74873.85 (3
mr30	-1740.55 (29)		-598.46 (38)		30031.85 (3
ms1	-673.36 (21)		811.01 (33)		38540.81 (3
ms001	-8421.58 (29)		-843.61 (23)		24139.00 (2
ms2		1027.03 (38)	5		38393.41 (
ms002	-7213.97 (23)	6697.63 (32)	1297.29 (34)	- L.	30150.72 (2
ms003	-7830.01 (25)		-894.86 (19)		24980.41 (1
ms4	-1159.36 (29)		603.37 (32)		7) GG.G0112
ms004	-6768.30 (23)	7030.34 (32)	1170.90 (25)		30510.76 (2
consm	-1182.43 (29)	132/131 (34)	(27) 04.40		3/4/2/4/2
mso	(77) /17 (77)	1497.52 (34)	-606.01 (37)		
ms006	-6698.04 (23)		2166.28 (38)		
ms/	-1403.03 (29)	1420.82 (34)	-/ ID.48 (34)	(75) 17/6CT05-	
msuu/		1865.08 (34)	-1339.11 (38)	-41050.14 (19)	/ 1920.69 (38
ms008	-1555.14 (29)				34202.05 (3
600su	-9530.34 (23)	9804.74 (36)	-1098.67 (23)		30381.35 (2
OTSU	(67) 10 10 10 10 10 10 10 10 10 10 10 10 10	4933.96 (32)	(55) 16.6641		
msulu	-8341.35 (19)	9842.1b (3b)	(38) 1539.54 (38)		
ms11	(67) 07 07 07 07 07 07 07 07 07 07 07 07 07	(25) 12.6000	(75) 57,5507-	- /8830.40 (34)	101130.4/ (32
TTOS	(CZ) 60'00+0T-	(0C) CU-1026	(6T) 00'+CTT-		
2TSU	-/114./4 (23)	(70) 71 0100	(96) 07:0402		1) 06'0700/
ms012	(61) / 1'9006-	9313.10 (30)	(9C) DC.88/T		2) C0./44/2
CTOSII	(67) 40' / CT-	(4C) CO'TOZT	(07) /1:077	(7C) 10'TC0TZ-	7) 70'0C017
514 5014	(6T) 00'TC24-				) 00%T0/4
mc1E	(67) 59/065T-	(4C) /C.771	(75) 87.678	(36) 62,30/ /2-	cc.401c2
mc015					2) LE 97020
mc016					
mc017	(62) 02:722-	(FC) /0'CCCT	356 75 (28)		2) CD 7744 02 (2)
ms018	-2041 61 (29)	1918 54 (34)	1943 15 (38)	-60420 02 (38)	45008.73 (38
ms019	-1950 20 (29)		7167 86 (38)		
ms020	-8093.86 (19)	9842.99 (36)	1759.74 (38)		49150.05 (28
ms021	-8758.68 (19)	9313.99 (36)	2160.76 (38)	2	
ms22	-4658.50 (29)		2090.27 (33)		
ms022	-7015.98 (23)	6698.29 (32)	1581.55 (34)		
ms23	-10093.68 (23)	9801.36 (36)	-2869.52 (32)		
ms023	-6570.31 (23)	7031.00 (32)	1343.46 (38)	-33916.01 (38)	
ms24	-8118.12 (19)	10061.79 (36)	2705.17 (34)		114103.53 (38
ms25	-5010.82 (25)	6651.25 (36)		-140859.91 (36)	58388.01 (17
ms26	-10972.03 (25)	9280.64 (36)	-3470.16 (36)	-110292.50 (38)	
ms27	-8758.02 (19)	9768.18 (36)	3415.61 (38)	-27431.72 (38)	93131.27 (38
ms28	-1153.82 (19)	2117.99 (38)	-999.77 (36)	-44243.07 (36)	45094.06 (33
ms29	-2148.95 (29)	1501.69 (38)	1307.29 (36)	-40948.64 (37)	71128.08 (38
ms30	-1759.74 (29)	1678.08 (34)	733.10 (32)	-22132.32 (32)	31971.46 (29
ms32	-1346.02 (19)	2249.44 (36)	-1314.21 (37)		24766.05 (32
ms33	-2128.61 (29)		-1594.18 (36)	-64731.45 (38)	44370.59 (34
pdb1	101.87 (15)		0.00 (29)	0.00 (18)	
pdb2	102.56 (15)		0.00 (25)	0.00 (22)	0.00 (25
pdb5	105.58 (15)	2256.05 (29)	0.00 (29)	0.00 (18)	
pdb6	107.00 (15)	2363.96 (25)	0.00 (25)	0.00 (22)	
pel	-1249.69 (35)	-0.43 (39)	0.00 (23)	0.00 (23)	
pe001	-296.34 (32)	209.66 (19)	0.00 (38)		0.00 (38
hez	(cc) +0.00/-	(CT) 06:0-	(ET) NN'N	(oc) nn:n	GT) 00'0
111/	-417.4X (34)	111111111111111111111111111111111111111	0.00 (38)	0.00 (37)	0.00 (38)

Result Cases					
.01-1.4D1					
.01-1.4D1		Name			QI
	ENVI				15
2.12-1.2D1+1.0S0+0.5W7	1005				11
14-1.2D1+1.6S0+0	5W2				18
.15-1.2D1+1.6S0+0.	5W4				19
3.16-1.2D1+1.6S0+0.5W5	.5W5				20
.17-1.2D1+1.6S0+0	.5W6				21
18-1.2D1+1.6S0+0.	5W/ 2M/2				77
21-1 2D1+1 6S1+0	50/1				24
22-1 2D1+1 6S2+0	5M/2				75
23-1.2D1+1.6S3+0.	5W3				26
24-1.2D1+1.6S4+0.	5W4				27
25-1.2D1+1.6S5+0.	5W5				28
26-1.2D1+1.6S6+0.	.5W6				29
3.27-1.2D1+1.6S7+0.5W7	.5W7				30
28-1.2D1+1.6S8+0.	.5W8				31
6.01-0.9D1+1.0W1					32
ZW0.1+1UR.0-20.0					33
6.04-0.9D1+1.0W3					35
6 05-0 9D1+1 0W5					36
6.06-0.9D1+1.0W6					37
6.07-0.9D1+1.0W7					38
6.08-0.9D1+1.0W8					39
Member Forces					
Member	Fx Min Ib	Fx Max Ib	≥ੁੁ	Mz Min Ib-in	Mz Max Ib-in
eb001	4783.69 (32	7566.97 (19		-4219.28 (38	222.32
eb002	4776.00 (32)	5464.39 (23)	1	-4983.57 (34)	3222.32 (34)
ebuus ahnn7	-4///.00 (32)	045.90 (29 0465 52 (75)	25.33 (34)	(45) / 5, 200 - 4903 - 200 - 20	2004.03 (38)
eh008	-6833 26 (36)	6652 36 (19)		-6970 44 (38)	4564 41 (38)
eb009	-6832.99 (36)	9178.44 (23)		-5209.05 (34)	4564.41 (38)
edb1	-2179.95 (29)	129.67 (34)		0.00 (34)	
lb2	-2163.65 (25)	109.28 (38)		0.00 (19)	0.00 (38)
edb5	-2732.94 (25)	182.03 (38)		0.00 (19)	0.00 (38)
edb6	-2618.12 (29)	134.49 (34)		0.00 (39)	0.00 (39
	-1224.49 (32)	1369.51 (29)		0.00 (35)	0.00 (38
2 2		1301.01 (29)		0.00 (38)	0.00 (35)
	-1220.51 (35)	124/.10(29)		0.00 (35)	0.00 (38)
4	(d2) 727 (30)	(82) 5/.0161		(35) 000	Z) 00'0
dh6	(32) 104 07 (32)	(07) 00 8616	0.00 (35)	0.00 (35)	(96) 00.0
gii0 m/001	-1282.70 (25)	1738.93 (32		-75251.26 (35)	61017.34 (3
002	-1282.62 (25)	1739.31 (32)		-53395.77 (38)	65837.06 (3
av003	-1251.52 (23)	2543.06 (34		-41499.25 (35)	33648.36 (3
gv004	-1251.84 (23)	2544.35 (34)		-26447.73 (35)	21449.96 (3
gv005	-2309.41 (25)	3766.36 (38)		-16.30 (38)	10.96 (35)
gv006		3766.99 (38)		-8.11 (38)	5.46 (35)
gv007	-1907.73 (23)	2662.22 (36)		-197.60 (35)	140.88 (38)
gv008	-1908.38 (23)	2663.64 (36)		-35.38 (38)	49.63 (35)
TJU	(17) 02/370 (70)	1234./2 (32)		(65) 00.020	(95) 50,68015
mr2	(67) 0/1041-	(0C) / C'CZOT (DC) DU 1211	(CE) 11 818	(CC) CC.02CH-	(0C) CH'C//TC
14	(22) 00'T /6-	1407 57 (34)	ľ	(CC) CC:0TO/-	73306 10 (33)
1.12	-1414.65 (29)	1419.16 (34)		-25601.97 (33)	55309.48 (34)
mr6	-1156.00 (29)	1327.92 (34)		-5217.00 (21)	16495.64 (32
mr7	4053.64 (29)	4933.96 (32		-75006.68 (21)	
mr8	-8972.60 (29)	6654.79 (32)	-3076.86 (32)	-75173.14 (21)	155591.48 (32)
mr9	L6286 55 /721				



# HTS F173 13M

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F173
HTS

Mombor	L Min	Ev Max	141		M-7 Min		VCM -M	
		lb lb	é, q	-	ni-di		Ib-in	
neß	-1057.04 (38)	-1.19 (28)	0.00 (38)			0.00 (38)	2	0.00 (19)
p 001	-566.76 (35)	428.56 (38)	0.00 (38)		0.00	(38)		0.00 (37
pl2	-135.19 (35)	89.67 (38)	0.00 (38)		0.00	0.00 (19)		0.00 (38)
pl002	-224.64 (35)	139.67 (38)	0.00 (38)		00.0	0.00 (38)		0.00 (37
pl3	-1408.23 (35)	465.03 (38)	0.00 (38)		00.0	0.00 (38)		0.00 (25)
pl003	-700.43 (19)	675.29 (38)	0.00 (38)		00.0	0.00 (38)		0.00 (37
pl4	-776.63 (19)	38.96 (34)	0.00 (34)		0.00	0.00 (34)		0.00 (38
pl004	-718.65 (35)	486.14 (38)	0.00 (38)		00.0	0.00 (38)		0.00 (37)
pl5	-848.32 (35)	667.43 (38)	0.00 (34)		0.00	0.00 (34)		0.00 (23)
02	-107.14 (35)	58.69 (38)	0.00 (38)		0.00	0 (37)		0.00 (3
pl6	-495.87 (35)	-35.70 (15)	0.00 (34)		0.00	0.00 (34)		0.00 (38
pl17	-648.56 (19)	63.72 (38)	0.00 (38)		0.00	0.00 (35)		0.00 (38)
pl18	-63.16 (35)	24.93 (38)	0.00 (38)		0.00	0.00 (35)		0.00 (3
6	-732.65 (35)	1.27 (39)	0.00 (38)		0.00	0.00 (24)		0.00 (38)
0	-289.56 (35)	202.61 (38)	0.00 (34)		0.00	0.00 (34)		0.00 (39)
p 21	-604.38 (38)	-30.56 (28)	0.00 (34)		00.0	0.00 (34)		0.00 (38)
wb1	0.82 (15)	1065.65 (38)	0.00 (32)		0.00	0.00 (32)		0.00 (32
wb2	38.28 (33)	1409.61 (35)	0.00 (32)		00.00	0.00 (34)		0.00 (32
	0.19 (15)	970 77 (38)	0.00 (38)		000	(38)		0 00 (3
wh4	1.13 (16)	1337 68 (35)	0.00 (34)		000	0.00 (34)		0.00 (32)
	62 51 (15)	677 63 (22)	0.00 (38)		000	0.00 (38)		0.00 (19)
wh6	3 13 (30)	766 14 (35)	0.00 (35)		000	0.00 (38)		0.00 (35)
	(0C) CT/C	(CC) 11 0C0			000	(00) 0000		
	(CT) /0.00	(3C) CT'6ZO				(00)		0T) 00 0
ouv of	(20) 60:602	(CC) 06'0CZT			000	(10)000		
	(07) 17:6	(GT) T / CLC			0.00	(00)		
DTOM	(07) //·T7	(00) 00.060	(20) 00.0		0.00	(10) 00.0		70) 0000
TTOM	(ET) C7:70	(6T) CU: /64	(97) 00 0		0.00	(cc) 00.0		07) 00 0
1 1	(TC) 76.70	(00) 00,000			0000	(00)		
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HTS tentiQ GmbH Hinter der SchlagmÃ1¼hle 1 63699 Kefenrod Germany

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A3 - Appendix C-HTS Hoecker.xmcd

Planning Worksheet	APP NO	20-01723	
No Inspections Required <b>O</b>	ADDRESS:	35 N. High Street	
	DATE:	9/18/20	
Updated in Naviline O	PLAN REVIEW	ER: Velma Coen	
Check All	Require	l Inspections	
Zoning Rough	ZONR	*	
Zoning Final	P18	(999)	$\overline{\mathbf{A}}$

\* Must come before Frame Inspection



Johnson Controls

3,5,6,7

## Series 5 (3-6 Ton)

Single Package R-410A Air Conditioner

Page: 19

#### Project Name: The Shops at Rocky Fork

### Unit Model #: JA6ZFN10U2AAB1

Quantily: 4 Tag #: Building B RTU-

System: JA6ZFN10U2AAB1 (4)

#### **Cooling Performance** Total capacity 68.8 MBH Sensible capacity 50.4 MBH Refrigerant type R-410A Efficiency (at ARI) Ambient DB temp. 11.00 EER 95 0 OF Entering DB temp. °F 80.0 Entering WB temp. 67.0 °F Leaving DB temp. °F 60.6 Leaving WB lemp. °F 58.0 Power input (w/o blower) 6.65 kW Sound power 82 dB(A) **Gas Heating Performance** Entering DB temp. 60 °F Heating output capacity (Max) Supply air 2400 CFM Heating input capacity (Max) Leaving DB lemp. 125 MBH 98.6 °F Air lemp. rise 38.6 °F AFUE 80.3 % Slages Supply Air Blower Performance Supply air 2400 CFM Ext. static pressure 0.6 IWG Unit static resistance 0.2 IWG Blower speed Max BHP of Motor (including service factor) 1290 RPM 3.45 HP Duct location Bottom Molor rating 3.00 HP Actual required BHP 1.72 HP Power input 1.61 kW Elevation 0 ft. BELT Drive type **Electrical Data** 208-3-60 Power supply Unit min circuit ampacity 37 Amps Unit max over-current protection 50 Amps **Dimensions & Weight** Hgt 33 in. Len Weight with factory installed options 33 in. Len 83 in. Wth 45 in. 770 lbs Clearances Right 24 in. 32 in. Front Back 36 in. Тор 72 in. Bollom 0 In. Left 36 in. Note: Please refer to the tech guide for listed maximum static pressures



#### 6 Ton

Johnson Controls Units are Manufactured at an ISO 9001 Registered Facility and Each Rooftop is Completely Computer-Run Tested Prior to Shipment.

#### **Unit Features**

- Unit Cabinet Constructed of Powder Painted Steel, Certified At 1000 Hours Salt Spray Test (ASTM B-117 Standards)
- Through-the-Curb and Through-The-Base Utility Connections
- Elther Supply and/or Return can be Field Converted from Vertical to Horizontal Configuration without Cutting Panels.
- Full Perimeter Base Rails with Built in Rigging Capabilities
- Galvanized Steel Drain Pan
- Scroll Compressor
- Single Stage Cooling
- Solid Core Liquid Line Filter Driers
- Microchannel Condenser Coil
  - 100 MBH Oulput Aluminized Steel, Single Stage Gas Nominal Heat
- 3 HP High Static Belt Drive Blower
- Unit Ships with 1" Throwaway Filters with a Standard Filter Rack That Will Accept up to 2" Filters
- Single Point Power Connection
- Phase Monitor
- Single Enthalpy Economizer and Hood (No Barometric Relief Damper) Short Circuil Current: 5kA RMS Symmetrical

#### Standard Unit Controller: Simplicity Control Board

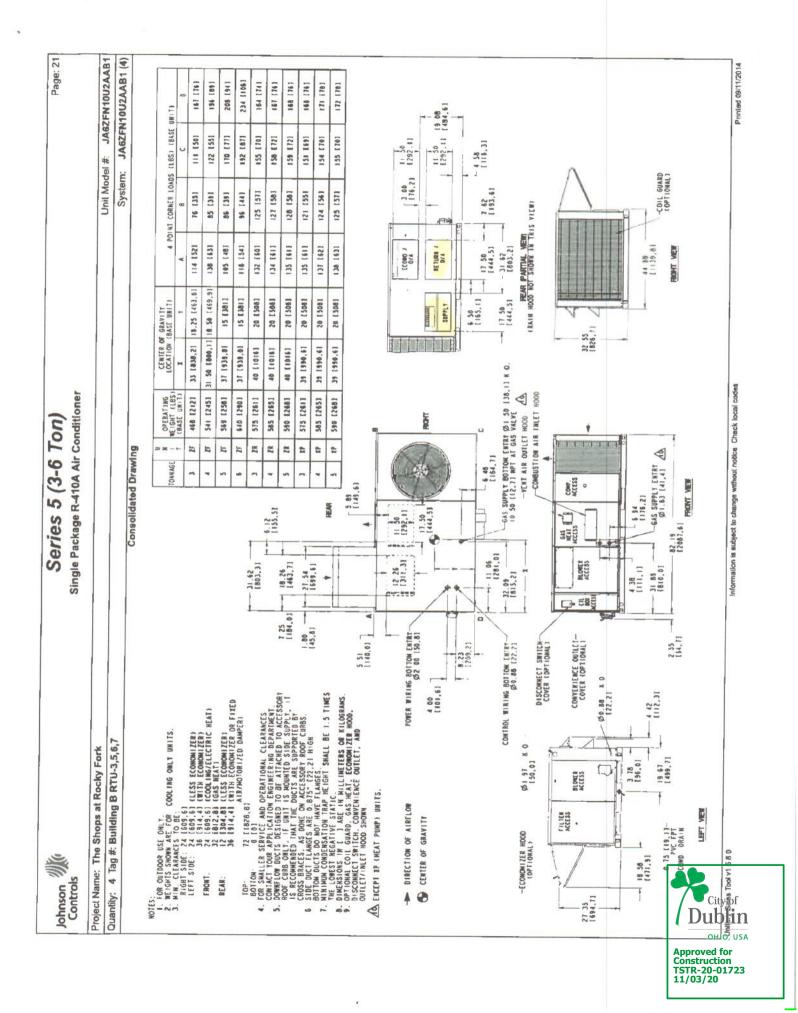
- · An Integrated Low-Ambient Control, Anti-Short Cycle Protection, Lead-Lag, Fan On and Fan off Delays, Low Vollage Protection, On-Board Diagnostic and Fault Code Display.
- Safety Monitoring Monitors the High and Low-Pressure Switches, the Freezestats, the Gas Valve, if Applicable, and the Temperature Limit Switch on Gas and Electric Heat Units. The Unit Control Board will Alarm on Ignition Failures, Safety Lockouts and Repeated Limit Switch Trips.

#### Warranty

- One (1) Year Limited Warranty on the Complete Unit
- · Five (5) Year Warranty Compressors and Electric Heater Elements
- · Ten (10) Year Warranty Aluminized Steel Tubular Heat Exchangers



JOHIISOH VAN		A Air Conditioner	Page: 2
Project Name: The Shops at Rocky Fork		Unit Mode	al #: JA6ZFN10U2AAE
Quantity: 4 Tag #: Building B RTU- 3,5,6,7		System:	JA6ZFN10U2AAB1 (
Factory In	stalle	d Options	
JA6ZFN	N10U	2AAB1	
		6 Ton	
Nominal Cooling Capacity:	JA6	Single Stage Cooling	
Product Category:	z	Johnson Controls Series 5 Single Pack Conditioner	aged R-410A Air
Product Identifier:	F	11.0 EER / 11.3 IEER	
Heat Type and Nominal Heat Capacity:	N10	100 MBH Output Aluminized Steel, Sing Heat	jle Stage Gas
Airflow:	U	3 HP High Static Belt Drive Blower 1" Throwaway Filters Single Enthalpy Economizer and Hood Relief Damper)	(No Barometric
Voltage:	2	208/230-3-60	
Installation Options:	A		
Additional Options:	AB	Microchannel Condenser Coil Phase Monitor Galvanized Steel Drain Pan	
Product Generation:	1		
<ul> <li>1RC0434 - Roof Curb - 14" High, Flat, Uninsulated, Full Perimeter (Shipped Knocked Down) (86.0 lbs)</li> <li>1RD0410 - Barometric Relief Damper with Hood Kit (Downflow Unit or Duct Mounted) (6.0 lbs)</li> <li>2EP07700424 - JCI Branded, 2 Heat / 2 Cool, Electronic 7 Day Programmable, T600MSP-3 (2.0 lbs)</li> </ul>			





### WASHINGTON TOWNSHIP FIRE DEPARTMENT

6200 Eiterman Road Dublin, Ohio 43016 614-652-3920

### Tent Application Process For Dublin 2017 Ohio Fire Code based upon the 2015 International Fire Code Rules and Regulations for Tent Installation

Permits are required for a <u>tent (capable of installing side curtains)</u> in excess of 200 sq. ft. or a <u>canopy (side curtain prohibited)</u> in excess of 400 sq. ft. Construction shall comply with the current Ohio Building Code and applicable provisions of Chapter 24 in the Dublin Fire Code.

- ☑ Place of assembly tents (50 or more persons) requires all of the following:
  - ✓ exit and emergency lighting
  - ✓ proper number of approved exits based on the occupant load
  - ✓ no open or exposed flames inside or within 20 feet of tent
- Free of straw, hay, shavings, or similar combustible materials
- NO SMOKING shall be permitted in tents or under canopies. Approved "No" Smoking signs must be posted.
- All tents and canopies shall be flame resistant treated and the proper certification along with proper labeling affixed on the material.
- ☑ All tents and canopies must be properly anchored. (City of Dublin requires caps on all steel stakes installed on city property.
- ☑ Fire extinguishers are required in cooking and place of assembly tents. (Minimum 5lb rated 2A-10BC)
- ☑ Cooking and heating equipment shall not be located within 10 feet of the exits or combustible materials.
- ☑ Flammable and combustible liquids must be stored outside in an approved manner not less than 50 feet away from structure.
- ☑ LP-gas containers 500 gallons or less shall have a minimum separation between the container and structure not less than 10 feet and properly secured to prevent unauthorized movement.
- ☑ LP-gas containers gallons or more shall have minimum separation between the container and structures of not less than 25 feet and properly secured to prevent unauthorized movement.
- ☑ Generators and other internal combustion power sources shall be separated from tents/canopies by a minimum of 20 feet and shall be isolated from contact with the public by fencing, enclosure or other approved means.
- ✓ Fees for tents and canopies are based on the number of tents or canopies installed #1-5 = \$50.00 #6-10 = \$75.00 #11-15 = \$100.00 #16-20 = \$160.00 #20+ = \$200.00
- ALL TENTS SHALL BE INSPECTED by the Dublin Building Division and the Washington Township Fire Department before occupancy.



#### TRUSTEES

Denise Franz King Charles W. Kranstuber Jan Rozanski

#### **FISCAL OFFICER**

Joyce E. Robinson

6200 Eiterman Road Dublin, Ohio 43016 0 614 652 3920

#### SITI DOUT DECIDED TO ACCELT

C	ity of Dublin Review Services - <i>THIS IS NOT A REVI</i>		
Application #	tSTR-20-01723	_ Submitted Date	10
Project Name	e Tucci's Patio Tent Winter	Project Address	
Project Cont	act E-mail		Phone
	Staff Use	Only Below This Line	
Received by	Review Services (Date) 9/11		
YES NO	Application Complete? (Date) 9/1 If not complete please review items ma	1 by: dt	f
	GENERAL- Actions Required (As Application Temporary Structures Form Com Design Professional Seals on Drawings/Docum No PRELIMINARY drawings included in submi Itemized response to previous reviews prov Drawings properly named and oriented.	plete ents tted Drawings/Documents	Reviewer Initials Reviewer Initials
YES NA NO	BUILDING/ELECTRICAL- Action Building Code Summary (construction type, oc Tent Floor Plans provided		
	Site Plan with distance from buildings to Te Platform with accessible exit(s). 2 accessible Flame Retardant Certificate for Tent Fabric Egress Illumination with Emergency Power Exits and exit access doors marked on the d Minimum Structural Loading provided Special Inspections provided (if required) Special Inspector's Credentials provided (Cre Toilet Fixtures complying with OBC 2902.1 a Delegated Design Listed and Phased Approv Generator located, sized and grounded show	exits if occupancy > 49 occupance > 49 occupance to provided on Drawing at 1 FC provided rawings provided (if require dentials required for any appr and OBC Chapter 11 provid al Request Form provided?	pants provided on Drawings. js/Documents d) roval) led
YES       NA       NO         Image: Im	FIRE - Actions Required Required Fire Protection Systems or Fire Wa Fire Extinguishers located on the drawings. ZONING/PLANNING - Actions R Site Plan provided ENGINEERING - Actions Require Site Plan provided	equired	Reviewer Initials Reviewer Initials BC Is CAS/df

### **PRESCREEN NOTES**

Show how the base plate will be anchored



City of

Approved for Construction TSTR-20-01723 11/03/20

## **PRESCREEN NOTES (Continued)**

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	 Approved for
	TSTR-20-01723 11/03/20

Washington Township Fire Department 6200 Eiterman Road Dublin,Ohio 43016 (614)652-3920

### Notice of Plan Review

Tucci's Restuarant 35 N High ST Dublin, OH 43017 Occupancy ID:000000184

Project: TUCCIS PATIO WINTER (TENT)
Application #: TSTR-20-01723

Use: A-2

Construction: N/A

Area: 1,949 SF

**Occupancy:** 62 - PER SEATING CHART

Notes: RECOMMENDED FIRE DISAPPROVAL OF THE TENT DRAWINGS.

Reported Dat	te Code/Description
09/16/2020	150 Permit
	3104.15 Heating and cooking equipment
	Notes:
	Heating and cooking equipment shall be in accordance with paragraphs
	(D)(15)(a)(3104.15.1) to (D)(15)(g)(3104.15.7) of this rule
	1. HOW WILL THIS STRUCTURE BE HEATED? - PROVIDE DETAIL OF ANY HEATING UNIT AND
	ITS POWER/FUEL SOURCE.
as to	E have reviewed the Construction Documents for the referenced project, s submitted to the Division of Building Standards for matters of concern o the Washington Township Fire Department pertaining to fire protection nd the 2017 Ohio Fire Code (OFC)

Inspector, Hamilton, Chad





### LISTING OF ITEMS OF NON-COMPLIANCE

### This is not a Building Permit. It is a record of our review of documents submitted with your application for a Building Permit.

23 September 2020

Ms. Brenda Kinser O'Neil Tents 895 W. Walnut Street Canal Winchester, OH 43110 (614) 837-6352 bjk@oneiltents.com

Re:	Tucci's Patio Winter Tent	
Address:	35 N. High Street (43017)	
Application No.:	TSTR-20-01723	

Dear Ms. Kinser:

The construction documents submitted 15 September 2020 have been reviewed for compliance with the provisions of the 2017 Ohio Building Code (August 2018 Edition). The review was based upon the following criteria:

Primary Use Group: Area/Occupant Load:	A-2 (Restaurant) 1,969 SF / Chairs @ Tables shown = 62 Seats* *Reference all current Governor of Ohio's "Responsible RestartOhio" regulations and guidance for social distancing requirements.
Construction Type:	TBD
Special Stipulations:	<ol> <li>Set up 1 November 2020: Take down by 29 April 2021 (&lt;180 days) or until the end of the executive Order, whichever is first.</li> </ol>
	<ol> <li>Tents must be evacuated if wind speeds meet or exceed 40 MPH.</li> </ol>
	2. No cooking allowed.
Project Description:	Temporary structure to create outdoor eating area for Tucci's restaurant as allowed by City of Dublin "Executive Order for Portable Structures and Temporary Uses" related to COVID-19 State of Emergency (March 17, 2020). Tent consists of a clear span 43'-0"x43'-0" structure and attached 10'x12' vestibule tent, all with closed sides.
Previous Occ Cert:	TSTR-20-00999 (summer tent); 12-200470 (building)

11/03/20

City of blin

OHIO, USA

LISTING OF ITEMS OF NON-COMPLIANCE- cont.

23 September 2020 Page 2 of 3

Tucci's Patio Winter Tent Application No. TSTR-20-01723

The construction documents were prepared by O'Neil Tents and Robert V. Wangia, Ohio registered engineer #E-73309 to comply with the requirements of the OBC Section 107.4.3 and have been reviewed, therefore, in accord with that Section.

**OBC 107.4 Review of plans**. When construction documents have been submitted to the building department for review and approval, the building official shall cause the construction documents to be examined for compliance with the rules of the board....

The construction documents, which have been submitted for review, do not allow the City of Dublin to issue a full approval. The following item(s) have been found to not be in compliance with the rules of the board:

- **Item 1 OBC 3103.1.1 Conformance.** Temporary structures and uses shall conform to the structural strength, fire safety, means of egress, accessibility, light, ventilation and sanitary requirements of this code as necessary to ensure public health, safety and general welfare.
- **Item 2 OBC 106.1.1 Information on construction documents.** Construction documents shall be dimensioned and drawn upon suitable material. Electronic media documents are permitted to be submitted when approved by the building official. Construction documents shall be coordinated and of sufficient clarity to indicate the location, nature and extent of the work proposed and show in detail that it will conform to the provisions of this code. Construction drawings shall include information necessary to determine compliance with the building, mechanical, plumbing and fire protection codes such as:
  - a. Please show the tent location (in relation to existing building and property lines) and orientation on the site plan, including location of the vestibule tent and access to the exit discharge.
  - b. Floor plans must show all relevant information such as, but not limited to, door locations, door swings and all portions of the means of egress.
    c. Please provide information for any proposed heating in this structure.
- c. Please provide information for any proposed heating in this structure.
   Item 3 OBC 602.1 General. Buildings and structures erected shall be classified in one
  - of the five construction types defined in Section 602.2 through 602.5.
  - a. Please provide Flame Retardant Certificate for Tent Fabric or other documentation to demonstrate and confirm construction type classification.
- **Item 4 OBC 1010.1 Doors.** Means of egress doors shall meet the requirements of this section. Doors serving a means of egress system shall meet the requirements of this section and Section 1022.2.
  - a. Please provide information for all egress doors including size, direction of swing, door operations, and hardware.
- **Item 5 OBC 906.1 Where required.** Portable fire extinguishers shall be installed in all of the following locations: 1. In Group A occupancies....
  - a. Please show size, type and location of portable fire extinguishers.
- **Item 6 OBC 1604.8 Anchorage.** Buildings and other structures, and portions thereof, shall be provided with anchorage in accordance with Section 1604.8.1 and 1604.8.3, as applicable.



N:\Building Standards\Commercial Reviews and Codes\Reviews 2019/TSTR-20-01723 n1 Tucci's Patio Winter Tent

LISTING OF ITEMS OF NON-COMPLIANCE- cont.

23 September 2020 Page 3 of 3

Tucci's Patio Winter Tent Application No. TSTR-20-01723

- a. The drawings indicate that (4) anchors are used in each base plate, but do not provide information for proposed anchors. Please show how the base plate will be anchored.
- **Item 7** The Washington Township Fire Department has requested an opportunity to provide input to the Dublin building department on issues relating to fire protection. The building official has evaluated the Department's comments related to the fire protection provisions of the OBC and incorporates those comments, by reference, into this Listing of Items of Noncompliance.
  - a. Please reply to and resolve the matters of the Fire Department's correspondence to this office.

Please advise the reviewer if the owner will cause the information to be provided to the department for review or dispute the items of noncompliance we have identified. If the owner's intention is to dispute an item of non-compliance, please provide the basis for the dispute for the building official's review. The building official shall evaluate your response, the plans examiner's report and any reports received from the fire official as described in Section 106.1.2.5 and render a final determination as to whether the items of noncompliance are to be communicated to the owner in the form of an adjudication order complying with Section 109. The building official shall also determine whether any further approvals are possible, and issue the appropriate approval as described in Section 105.

Please provide a written, point by point response, identifying the action or position taken to each of the items and sub-items in the listing.

Reviewed and Signed,

### J.E. Rusanowsky

Janet E. Rusanowsky, Architect Commercial Plans Examiner (614) 410 4612 jrusanowsky@dublin.oh.us

Owner or Owner's Representative

Date

Print Name and Title as Signed



N:\Building Standards\Commercial Reviews and Codes\Reviews 2019/TSTR-20-01723 n1 Tucci's Patio Winter Tent



GEOTECHNICAL CONSULTANTS INC.

TSTR-20-01723

MAIN OFFICE 720 Greencrest Drive Westerville, OH 43081 614.895.1400 phone 614.895.1171 fax YOUNGSTOWN OFFICE 8433 South Avenue Building 1, Suite 1 Boardman, OH 44514 330.965.1400 phone 330.965 1410 fax DAYTON OFFICE 2380 Bellbrook Avenue Xenia, OH 45385 937.736.2053 phone

www.gci2000.com

### FOOTING OBSERVATION REPORT

PROJECT:	Tucci's Outdoor Canopy 25 N High St - Dublin, OH	<b>DATE:</b> 11/04	/20 JOB NO.:	20-F-24684
CLIENT:	Lehman Daman Construction	WEATHER: S	Sunny, 60's to 70's	

#### **OBSERVATIONS:**

Footing soils were evaluated visually for foundation support. Soil bearing at footing elevation was verified using applicable testing methods and procedures. The following test data and observations were determined.

1) FOOTING LOCATION:	35 N High Street - Perimeter canopy augured pier footings at lines 1-4/A-D
2) PERMIT NUMBER: (If Applicable)	N/A
3) FOOTING ELEVATION (DESIGN / UNDERCUT):	Design
<li>4) FOOTING BEARING ON (FILL / NATURAL):</li>	Natural
5) VISUAL SOIL CONDITIONS:	Limestone bedrock
6) AVERAGE SOIL BEARING (P.S.F.):	5,000+
7) REQUIRED SOIL BEARING (P.S.F.):	3,000
<ul> <li>8) CONCRETE TEST CYLINDERS CAST? (YES / NO):</li> <li>9) COMMENTS:</li> </ul>	No

9) COMMENTS:

Observations indicated firm and stable soil conditions at footing grade. Observations indicated footing subgrade soil bearing values exceed required bearing values. Footings were excavated to approved project plan dimensions and reinforcing steel was installed per on site approved project plans (Page S1, dated 09/25/20, and submitted by Schaefer Architects).



## **Commercial Temporary Structure (Tents) includes WTFD Permit**

**JOB INFORMATION** 

Date: 11/03/2020

Record ID/ Permit No.: TSTR-20-01723

Address: 35 N HIGH St, DUBLIN, OH 43017

Type: Commercial Temporary Structure (Tents) includes WTFD

Job Name: Tucci's Patio Tent - Winter

Description: Installing a 43x43 clear span tent over the patio. Tent will be enclosed for winter seating for the restau

**Contractor:** 

Water Tap Size:

#### **APPLICANT RESPONSIBILITY**

I hereby agree that I will take full responsibility as required by law for compliance with all state and local codes and ordinances pertaining to construction and the conditions of this permit. All construction debris must be removed by the contractor. I also agree to notify the building department when work is ready for inspection and comply with section 108 of the Ohio Building Code for non-residential construction or the Residential Code of Ohio for Residential Construction.

#### **PERMIT ISSUED BY**

**Issued By:** 

Brad Fagell

City of Dublin Building Standards, 5200 Emerald Parkway - Annex, Dublin, Ohio 43017

Phone: 614.410.4670



STR -20 -61723



MAIN OFFICE 720 Greencrest Drive Westerville, OH 43081 614.895.1400 phone 614.895 1171 fax YOUNGSTOWN OFFICE 8433 South Avenue Building 1, Suite 1 Boardman, OH 44514 330 965.1400 phone 330.965.1410 fax DAYTON OFFICE 2380 Bellbrook Avenue Xenia, OH 45385 937.736 2053 phone

www.gci2000.com

November 20, 2020

Mr. Seth Burner Lehman Daman Construction 975 Eastwind Drive, Suite 130 Westerville, Ohio 43081

Reference: Special Inspections Summary Tucci's Outdoor Canopy 35 North High Street – Dublin, Ohio GCI Project No.: 20-F-24684

Dear Mr. Burner:

Geotechnical Consultants, Inc. (GCI) observed construction operations and performed materials testing from the period of November 4, 2020 to November 10, 2020 for the above referenced project. Services are on-going and a separate summary will be submitted at completion.

The foundations we observed were constructed on limestone bedrock. Our field reports noted that foundation subgrade bearing met or exceeded the required soil bearing pressure of 3,000 psf. Our observations further indicate that foundation steel reinforcement and dimensions were in accordance with the approved building plans and specifications. Compressive strength tests taken during foundation concrete placement met or exceeded design strength. Drilled anchor bolt placement (Hilti) was performed per the approved plans and the manufacturer's instructions.

We also observed placement of non-shrink grout under column bases to be satisfactory.

Specific information regarding our daily site visits can be obtained from our *Daily Site Observation Reports* for the project.

In summary, based on our site observations, it is our opinion that the referenced items were constructed in accordance with the approved project plans and specifications. We trust this letter provides you with the necessary information. If you have any questions or need additional information, please call.

Respectfully submitted, Geotechnical Consultants, Inc.

Robert L. Hiles, III Vice President



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Washington Township Fire Department 6200 Eiterman Road Dublin,Ohio 43016 (614)652-3920

### Notice of Plan Review

Tucci's Restuarant 35 N High ST Dublin, OH 43017 Occupancy ID:000000184

Project: TUCCI'S PATIO WINTER TENT, REV.

**Application #:** TSTR-20-01723(1)

**Use:** A-2

Construction: N/A

Area: 1,949 SF

**Occupancy:** 62 PER SEATING CHART

Notes: RECOMMENDED FIRE APPROVAL OF THE REVISED DRAWINGS.

#### Reported Date Code/Description

10/26/2020 130 Building 6801.01 No Violations Noted Notes: No Violations Noted.

REVISION 1 REVIEWED - COMPLIANT

\_\_\_\_\_

WE have reviewed the Construction Documents for the referenced project, as submitted to the Division of Building Standards for matters of concern to the Washington Township Fire Department pertaining to fire protection and the 2017 Ohio Fire Code (OFC)

Inspector, Hamilton, Chad



\* Denotes Violations Corrected or Variance Issued



### **CERTIFICATE OF PLAN APPROVAL**

This is not a Building Permit. It is a record of our review of documents submitted with your application for a Building Permit.

26 October 2020

Ms. Brenda Kinser O'Neil Tents 895 W. Walnut Street Canal Winchester, OH 43110 (614) 837-6352 <u>bjk@oneiltents.com</u>

Re:	Tucci's Patio Winter Tent		
Address:	35 N. High Street (43017)		
Application No.:	TSTR-20-01723(1)		

Dear Ms. Kinser:

The construction documents dated 25 September 2020 have been reviewed for compliance with the provisions of the 2017 Ohio Building Code (August 2018 Edition). The review was based upon the following criteria:

Primary Use Group: Area/Occupant Load:	A-2 1,849 SF / Chairs @ Tables shown = 62 Seats* *Reference all current Governor of Ohio's "Responsible RestartOhio" regulations and guidance for social distancing requirements
Construction Type:	IIB
Special Stipulations:	<ol> <li>Set up 1 November 2020; Take down by 29 April 2020 (&lt;180 days) or until the end of the Executive Order, whichever is first.</li> <li>This approval is for the 43'x43' main tent only.</li> <li>No cooking allowed.</li> </ol>
Project Description:	Temporary structure to create additional eating area for Tucci's restaurant as allowed by City of Dublin "Executive Order for Portable Structures and Temporary Uses" related to COVID-19 State of Emergency (March 17, 2020). Tent consists of a clear span 43'-0"X43'-0" enclosed, heated structure anchored to new concrete piers with two illuminated exit signs/egress lights w battery back-up and 2 fire extinguishers.
Previous Occ Cert:	TSTR-20-00999 (summer tent): 12-200470 (building)

The construction documents were prepared by Robert V. Nangia, Ohio registered engineer #E-73309 and Jeffery R. Bolchalk, Ohio registered engineer #E-70796 to comply with the

11/03/20

City of Dublin

#### **CERTIFICATE OF PLAN APPROVAL** - cont.

26 October 2020 Page 2 of 4 Tucci's Patio Winter Tent Application No. TSTR-20-01723(1)

requirements of the OBC Section 107.4.3 and have been reviewed, therefore, in accord with that Section.

**OBC 107.5.1 Approval of construction documents.** . . . When the construction documents have been determined to conform to the applicable provisions of the rules of the Board, the building official shall endorse or stamp such plans as approved and issue the certificate of plan approval in accordance with section 105.5.

#### Item 1 THE CONSTRUCTION DOCUMENTS ARE APPROVED

Item 2 The qualification of Geotechnical Consultants, Inc. as the Special Inspection company for all foundation and structural work has been reviewed and accepted by the building official.

**1704.2.4 Report requirement.** *Special inspectors* shall keep records of inspections. The *special inspectors* shall submit reports of special inspections and tests to the building official and to the registered design professional in responsible charge. Reports shall indicate that work inspected or tested was or was not completed in conformance to approved construction documents. Discrepancies shall be brought to the immediate attention of the contractor for correction. If they are not corrected, the discrepancies shall be brought to the attention of the building official and to the registered design professional in responsible charge prior to the completion of that phase of the work. A final report documenting required special inspections and tests, and correction of any discrepancies noted in the inspections or tests, shall be submitted at a point in time agreed upon prior to the start of work by the owner or the owner's representative to the building official prior to the *issuance of a certificate of occupancy*.

# This APPROVAL is for the issuance of a general building permit only. Separate permits and fees for plumbing, mechanical, sprinkler, electric and low-voltage must be obtained from the Dublin Building Standards Division prior to the start of any work in these generally subcontracted areas.

The following items are required for code compliance, but are not necessarily covered in detail in the construction documents. This list is a reminder to the design professional and contractors of issues, which are to be satisfactorily dealt with in the field:

- **Item A** Review and Approval of Plumbing Drawings and inspection of Plumbing installations are performed by the Franklin County Board of Health
- Item B OBC 106.3 Amended construction documents. If substantive changes to the building are contemplated after first document submission, or during construction, those changes must be submitted to the building official for review and approval prior to those changes being executed. The building official may waive this requirement in the instance of an emergency repair, or similar instance.



N:\Building Standards\Commercial Reviews and Codes\Reviews 2019/TSTR-20-01723(1) a1 Tucci's Patio Winter Tent

#### **CERTIFICATE OF PLAN APPROVAL** - cont.

26 October 2020 Page 3 of 4

Tucci's Patio Winter Tent Application No. TSTR-20-01723(1)

- **OBC 107.5.2 Posting.** The certificate of plan approval shall be posted in a Item C conspicuous location on the site. The owner and the contractor shall preserve and keep the certificate posted until the final inspections are complete.
- Item D OBC 107.7 Approved construction document sets. One set of construction documents shall be kept by the building official. The other set(s) shall be returned to the applicant, kept at the work site along with manufacturers' installation instructions and product information, and shall be available for use by the inspector.
- Item E **OBC 108.1 General.** . . . Construction or work for which an approval is required shall be subject to inspection by the building official. It shall be the duty of the owner or the owner's duly authorized representative to notify the building department when work is ready for inspection. Access to and means for inspection of such work shall be provided for any inspections that are required by this code.

It shall be the duty of the owner or the owner's authorized representative to cause the work to remain accessible and exposed for inspection purposes . . . until the work has been inspected to verify compliance with the approved construction documents. . .

This includes firestopping and draftstopping, mechanical work; piping, ducts and systems, structural members and connections, and electrical work (Chapter 27 OBC). All systems and elements covered by code are to be inspected and approved before being covered.

Subsequent work is allowed to proceed only to the point of the next required inspection.

- **OBC 804.3 Testing and Identification** Interior floor finish and floor covering Item F materials shall be tested by an approved agency in accordance with NFPA 253 and identified by a hang tag or other suitable method so as to identify the manufacturer or supplier and style, and shall indicate the interior floor finish or floor covering classification according to Section 804.2. Carpet-type floor coverings shall be tested as proposed for use, including underlayment. Test reports confirming the information provided in the manufacturer's product identification shall be furnished to the building official upon request.
- OBC 1101.2 Design. Buildings and facilities shall be designed and constructed Item G to be accessible in accordance with this code and ICC 117.1 as amended in Section 1112 of this chapter.
- All electrical will comply with the requirements of Article 27 OBC and the National Item H Electrical Code, NFPA 70, OBC approved.

Reviewed and Signed,

## J.E. Rusanowsky

Janet E. Rusanowsky, Architect **Commercial Plans Examiner** (614) 410 4612 irusanowsky@dublin.oh.us

Brad Fagrell Brad Fagrell, P.E.

Director of Building Standards/CBO



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## **CERTIFICATE OF PLAN APPROVAL** - cont.

26 October 2020 Page 4 of 4 Tucci's Patio Winter Tent Application No. TSTR-20-01723(1)

Owner or Owner's Representative

Date

Print Name and Title as Signed



N:\Building Standards\Commercial Reviews and Codes\Reviews 2019/TSTR-20-01723(1) a1 Tucci's Patio Winter Tent

CHECKLIST	<b>OF REQUIRED INSPECTIONS</b>
	Data: 26 Oct 20

	CHECKLIST OF REQUIRED INSPECTIONS					
	City of Date: 26-Oct-20					
	Dublin	blin Reviewer: jer				
	OHIO, USA	App Type Code: <b>TSTR</b>				
	INSPECTION <b>NOT REQUIRED</b>	А	pplication No: TSTR-20-01723(1)			
0	INSPECTION TO BE REQUIRED	P	Project Name: Tucci's Patio Wiinter Tent			
•	INSPECTION REQUIRED THIS PHASE					
	FULL APPROVAL	Proj	ect Address: 35 N. High Street			
	TYPE OF INSPECTION		TYPE OF INSPECTION			
	Building Inspections		HVAC Inspections			
•	FOOTINGS		HVAC ABOVE CEILING			
	FOUNDATION STEEL		HVAC ROUGH			
	FOUNDATION		HVAC FINAL			
	BUILDING PIERS		HOOD SUPPRESSION			
	BUILDING WATERPROOFING		Gas Piping Inspections			
	MASONRY WALL GROUTING		GAS PIPING UNDERGROUND			
	DIAMONDS (BOX OUTS)		GAS PIPING ROUGH			
	PRE SLAB		GAS PIPING FINAL			
	FIRE-RATED ASSEMBLY		GAS FIREPLACE			
	SHEAR WALLS		Franklin County Plumbing			
•	STRUCTURE / FRAME		PLUMBING UNDERGROUND			
	RATED WALL FASTENERS		PLUMBING ROUGH			
	FIREPLACE		PLUMBING FINAL			
	EXTERIOR WALL INSULATION		Washington Twp Fire Inspections			
	SHAFT WALL	•	FIRE PREVENTION			
	FIRESTOP ASSEMBLY		FIRE ALARM ROUGH			
	STRUCTURAL ABOVE CEILING		FIRE ALARM FINAL			
	WITNESS		SPRINKLER ROUGH			
•	OCCUPANCY		SPRINKLER ABOVE CEILING			
	Electrical Inspections		SPRINKLER FINAL			
	ELECTRIC TEMP SERVICE		FIRE LINE UNDERGROUND			
	ELECTRIC UNDERGROUND Additional Permits Required					
	ELECTRIC BONDING (UFER)					
	ELECTRIC ROUGH	PLUMBING				
	ELECTRIC ABOVE CEILING	HVAC				
	ELECTRIC SERVICE	GAS PIPING				
	ELECTRIC FINAL LOW VOLTAGE					
	Miscellaneous Inspections		FIRE PROTECTION			
	TENT		Certificate Type			
	DEMOLITION	•	CERTIFICATE OF OCCUPANCY			
			CERTIFICATE OF COMPLETION			



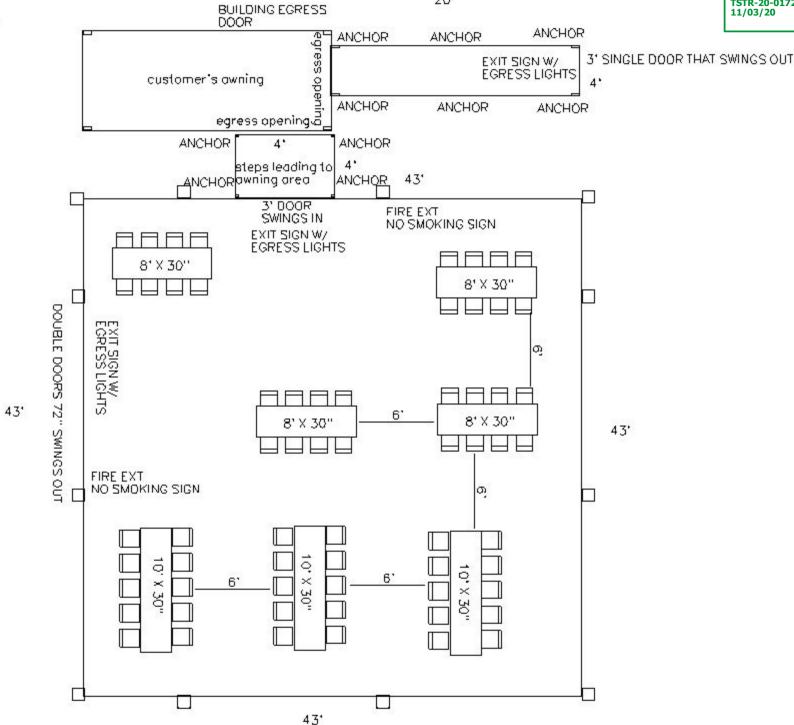
43X43 CLEAR SPAN TENT WALL ON ALL SIDES TENT WILL HAVE TWO ILLUMINATED EXIT W/EGRESS FIRE EXTGUISHERS 5 Ib ( 3–A 40 B–C) AND NO SMOKING SIGNS

ALL OCCUPANTS HAVE ACCESS TO RESTROOMS IN THE BUILDING

> = BASE PLATE AT EVERY UPRIGHT USES FOUR ANCHORS

4X4 CANOPY WITH WALL ON 4' SIDES ONLY. THIS TENT JUST COVERS THE AREA FROM THE TENT TO THE AWNING AND CONTAINS A SINGLE DOOR THAT SWINGS INWARD PER CITY SUGGESTION FRON ON SITE MEETING THIS TENT TO BE SECURED WITH SINGLE ANCHORS AT THE CORNERS

4'X20' WALKWAY TENT THAT WILL HAVE SIDE WALLS AND IT WILL CONNECT THE AWNING COVERED AREA AND RUN DOWN THE RAMP WITH A DOOR SWINGING OUT ON THE END THE TENT WILL BE SECURED WITH ANCHORS INSTALLED IN THE CONCRETE.

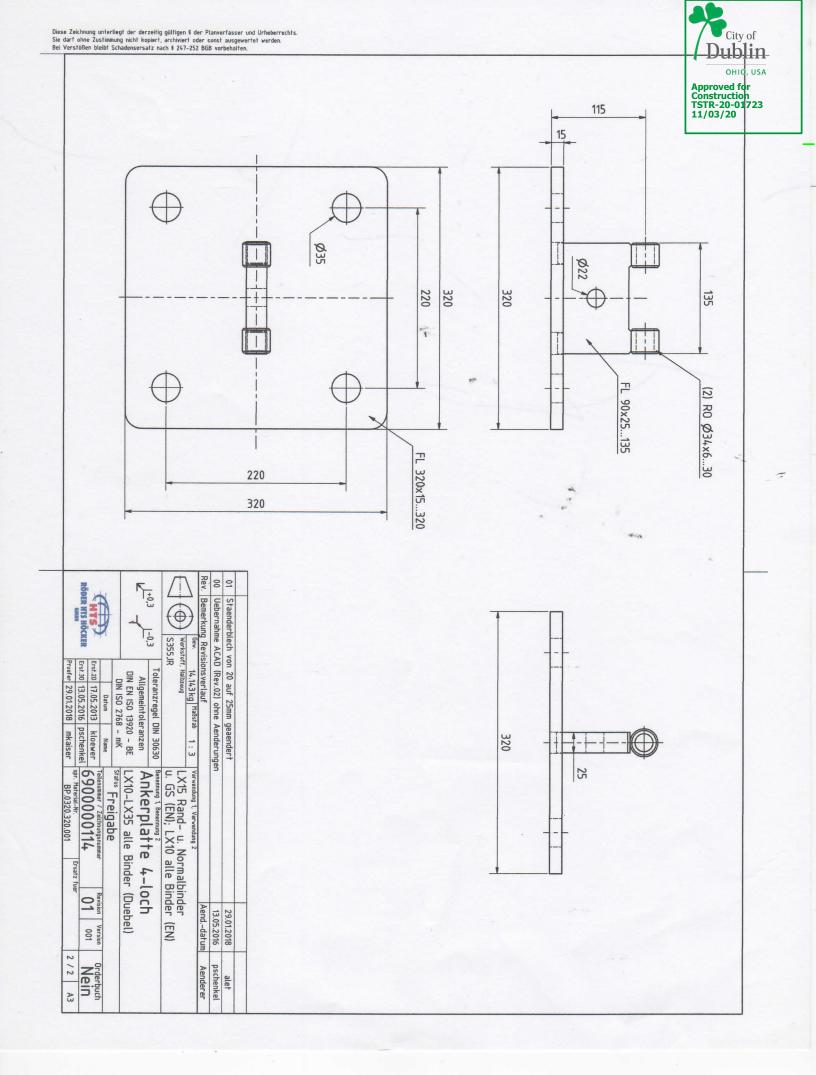


STREET SIDE

20'





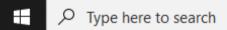


≡ 附 Gmail	Q Search mail			
- Compose				
Inbox 3	Re: Tucci tent Inbox ×			
★ Starred	Victor Manzano <victor.manzano@hts-tentiq.com></victor.manzano@hts-tentiq.com>			
Snoozed	to me -			
► Sent	Brenda,			
Drafts	Door specs below.			
Trash				
ΔΜΔΖΟΝ	width 1.185 mm			
Meet	height 2.140 mm Material Aluminium			
Start a meeting	Sash and frame color white			
	Filling VSG 6mm clear			
🥅 Join a meeting	Bottom cover (kicker panel) Without			
Hangouts	Fittings double wing door No double wing door Demountable No			
	Stop direction (from outside) DIN right			
Brenda - +	Number of door closers 1 door closer			
	Variants left and right aluminum rectangular tube 50x30x2mm			
	Fittings for single doors Active wing: inside Panic bar/external lever handle			
	Fittings Party tent door No party tent door Component single wing door			
	Best regards			
	Victor Manzano			
	Sales Manager US mid states & Canada.			
No recent chats	HTS-TENTIQ			
Start a new one	4328, E Tradewinds Avenue Lauderdale By Sea			
	Florida, 33308			
	USA			
	Cell +1 561 665 1199			

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Phone +1 561 450 6974

E-Mail victor.manzano@hts-tentiq.com



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				5,50/2020	

## **STRUCTURAL NOTES**

## **GOVERNING CODE**

2017 OHIO BUILDING CODE (REFERENCES IBC 2015 & ASCE-7 10).

DESIGN LOADS

1. TENT STRUCTURE FOUNDATION: FOUNDATION DESIGN IS BASED ON FOUNDATION RE PROVIDED BY HTS TENTIQ, DATED AUGUST 31, 2020

## **CONSTRUCTION AND SAFETY**

- 1. ENGINEER SHALL NOT BE RESPONSIBLE FOR THE MEANS, METHODS, TECHNIQUES, SEQUENCES OR PROCEDURES OF CONSTRUCTION SELECTED BY CONTRACTOR.
- 2. THE CONTRACTOR WILL BE SOLELY AND COMPLETELY RESPONSIBLE FOR CONDITIONS OF THE JOB SITE INCLUDING SAFETY OF ALL PERSONS AND PROPERTY DURING PERFORMANCE OF THE WORK. THIS REQUIREMENT WILL APPLY CONTINUOUSLY AND IS NOT LIMITED TO NORMAL WORKING HOURS. WHEN ON SITE, THE ENGINEER IS RESPONSIBLE FOR HIS/HER OWN SAFETY BUT HAS NO RESPONSIBILITY FOR THE SAFETY OF OTHER PERSONNEL OR SAFETY CONDITIONS AT THE SITE.
- CONTRACTOR SHALL BRACE ENTIRE STRUCTURE AS REQUIRED TO MAINTAIN STABILITY UNTIL 3 COMPLETE AND FUNCTIONING AS THE DESIGNED UNIT.
- 4. ANCHOR RODS AND FOUNDATION DOWELS SHALL NOT BE REPAIRED, REPLACED OR FIELD-MODIFIED WITHOUT THE WRITTEN APPROVAL OF THE STRUCTURAL ENGINEER OF RECORD.

## **FOUNDATIONS**

- 1. PER CLIENT'S REQUEST, THE FOUNDATION DESIGN AND GENERAL FOUNDATION NOTES ARE BASED ON THE ASSUMPTION OF FAVORABLE SOIL CONDITIONS. ALL FOOTINGS SHALL BEAR ON LEVEL (WITHIN 1 IN 12) UNDISTURBED SOIL OR APPROVED ENGINEERED FILL. FOUNDATIONS HAVE BEEN DESIGNED FOR A MAXIMUM SOIL BEARING PRESSURE OF 1500 PSF BELOW ISOLATED COLUMN FOOTINGS. FOUNDATIONS HAVE BEEN DESIGNED FOR A MAXIMUM LATERAL BEARING PRESSURE OF 150 PSF/FT BELOW NATURAL GRADE AGAINST PIERS.
- CONTRACTOR SHALL CONTACT UTILITY COMPANIES FOR LOCATING UNDERGROUND SERVICES AND 2 IS RESPONSIBLE FOR THEIR PROTECTION AND SUPPORT.
- FROST DEPTH IS 32 INCHES BELOW GRADE. BOTTOM OF FOOTINGS MUST BE BELOW SPECIFIED MINIMUM FROST DEPTH AS MEASURED FROM EXTERIOR GRADE. MAINTAIN SPECIFIED T/FDN ELEVATIONS AND THICKEN FOOTING OR PLACE ON CLSM AS REQUIRED.
- 4. FOUNDATIONS MAY BE PLACED WITHOUT SIDE FORMS IF EXCAVATED WALLS STAND APPROXIMATELY VERTICAL

## CAST-IN-PLACE CONCRETE (03-30-00)

- 1. CONCRETE MATERIALS:
- A. CONCRETE FOR FOOTINGS: f'c = 3000 PSI
- B. REINFORCING STEEL:
- i. DEFORMED BARS: ASTM A615,60 KSI YIELD.
- 2. REINFORCING BARS SHALL HAVE CLEAR COVER AS INDICATED ON THE DRAWINGS. WHERE NOT INDICATED, PROVIDE MINIMUM CLEAR COVER PER ACI-318
- 3. REINFORCING BARS SHALL BE FREE OF DIRT AND FORM RELEASE AGENTS.
- 4. CONCRETE WORK IN COLD WEATHER SHALL CONFORM TO ALL REQUIREMENTS OF ACI 306.1-90 "STANDARD SPECIFICATION FOR COLD WEATHER CONCRETING" AND ACI 306R-16 "GUIDE TO COLD WEATHER CONCRETING".
- CONCRETE WORK IN HOT WEATHER SHALL CONFORM TO ALL REQUIREMENTS OF ACI 305.1-14 "SPECIFICATION FOR HOT WEATHER CONCRETING" AND ACI 305R-10 "GUIDE TO HOT WEATHER CONCRETING". THE AIR TEMPERATURE, RELATIVE HUMIDITY, CONCRETE TEMPERATURE, AND WIND SPEED SHALL BE ENTERED INTO NOMOGRAPH FIGURE 4.2 IN ACI 305R-10 TO DETERMINE IF PRECAUTIONS AGAINST PLASTIC SHRINKAGE ARE REQUIRED.

## POST INSTALLED ANCHORS

- 1. INSTALLATION: INSTALL ANCHORS PER EVALUATION REPORT AND MANUFACTURER'S PRINTED INSTALLATION INSTRUCTIONS (MPII).
- CONNECTIONS TO EXISTING REINFORCED CONCRETE OR MASONRY: PRIOR TO DRILLING, VERIFY 2 LOCATIONS OF EXISTING REINFORCING BARS USING A REBAR DETECTOR. NOTIFY ENGINEER PRIOR TO INSTALLATION IF ANCHOR LOCATIONS CONFLICT WITH EXISTING REINFORCING BARS. DO NOT DRILL THROUGH REINFORCING BARS.
- TESTING AND INSPECTION: REFER TO EVALUATION REPORTS FOR ADDITIONAL TESTING AND 3 INSPECTION REQUIREMENTS.
- 4. SUBSTITUTIONS: SUBSTITUTIONS COMPLYING WITH SPECIFIED ACCEPTANCE CRITERIA MAY BE CONSIDERED. SUBMIT EVALUATION REPORT DEMONSTRATING COMPLIANCE WITH GOVERNING CODE AND SPECIFIED ACCEPTANCE CRITERIA PRIOR TO INSTALLATION.
- 5. ADHESIVE ANCHORS:
- A. ANCHOR RODS: HILTI "HAS-V-36" ASTM F1554, GRADE 36 UNLESS NOTED OTHERWISE. SIZE AND EMBEDMENT AS INDICATED ON DRAWINGS
- B. ADHESIVE IN CONCRETE: HILTI "HIT-RE 500 V3" EPOXY (EVALUATION REPORT: ICC-ES ESR-3814) OR HILTI "HIT-HY 200-A" HYBRID ADHESIVE (EVALUATION REPORT: ICC-ES ESR-3187). SUBSTITUTES COMPLYING WITH ACCEPTANCE CRITERIA ICC-ES AC308 AND ACI 355.4 FOR USE IN CRACKED CONCRETE MAY BE CONSIDERED.
- C. VERIFY THAT THE SHELF LIFE OF THE ADHESIVE HAS NOT BEEN EXCEEDED ON THE DATE OF INSTALLATION.

## SPECIAL INSPECTIONS

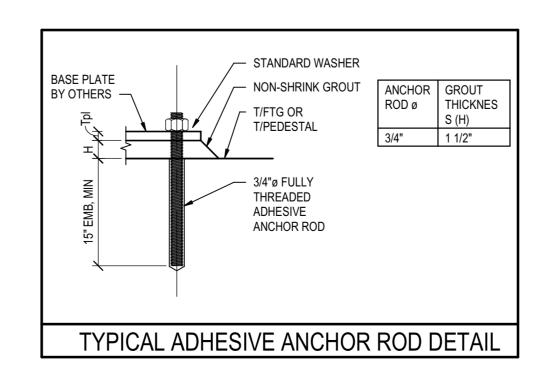
1. IT IS ASSUMED THAT SPECIAL INSPECTIONS ARE NOT REQUIRED, AND THAT THIS PROJECT MEETS THE EXCEPTIONS OF 1704.2 OF THE REFERENCED BUILDING CODE.

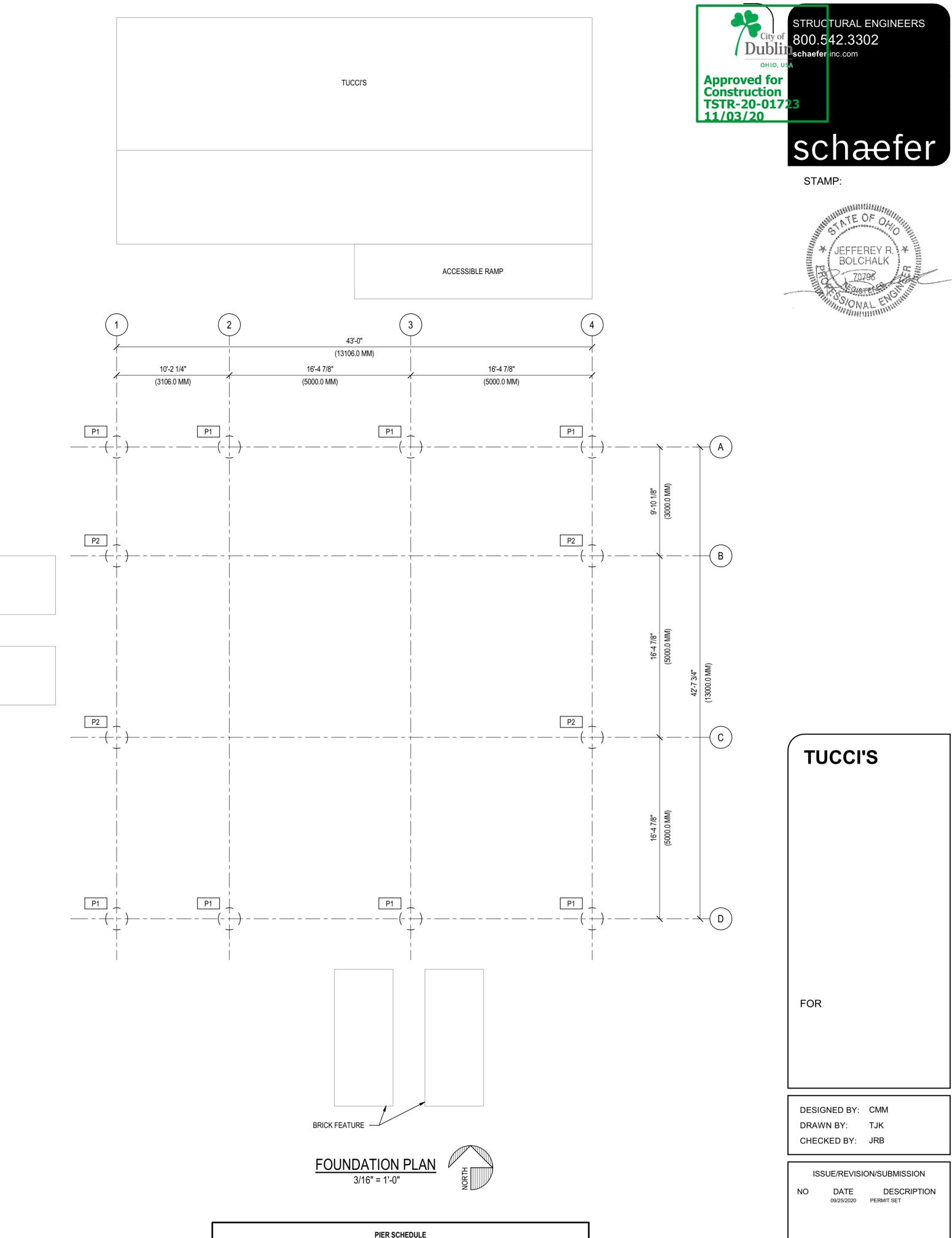
> DESIGN OF TENT SYSTEM SUPERSTRUCTURE & BASE PLATES SHALL BE PROVIDED BY THE TENT SUPPLIER

EACTIONS	

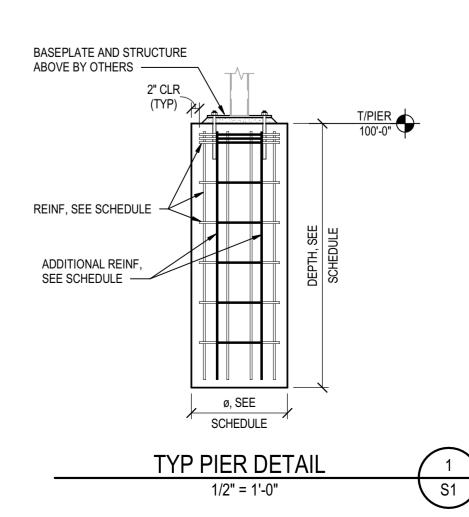
LEGEND DESCRIPTION REFERENCE SYMBOL n) COLUMN LINE DESIGNATION Pn PIER MARK SHEET S1 

BRICK FEATURE





PIER SCHEDULE					
REINFORCING					
MARK	ø	DEPTH	VERTICAL BARS	TIES	REMARKS
P1	2'-0"	5'-6"	(8) #5	#3 @ 10"oc w/ (3) TIES IN TOP 5"	PROVIDE ADDITIONAL (1) 180° BENT #5 BAR WITHIN 2" OF EACH ANCHOR ROD
P2	2'-0"	8'-0"	(8) #5	#3 @ 10"oc w/ (3) TIES IN TOP 5"	PROVIDE ADDITIONAL (1) 180° BENT #5 BAR WITHIN 2" OF EACH ANCHOR ROD





PROJECT NUMBER: 2014.87 SHEET NAME: GENERAL NOTES, **PLAN & DETAIL** DATE: 09/25/2020 SHEET: **S1** 

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Sattler PRO-TEX GmbH | Sattlerstraße 45 | 8077 Gössendorf, Austria

Unser Zeichen	Durchwahl	Gössendorf,
КОР	1532	29.09.2020

#### NFPA 701

We hereby confirm that the National Fire Prevention Association No. 701 Small Scale (Test 1) and Large Scale (Test 2) compliance documents are still valid:

- Flammability Test Report, Lab Identification no. 8543 •
- Flammability Test Report, Lab Identification no. 10316 •

**Kind Regards** 

Hoa Kongliger

i.A. DI Petra Königshofer **Product Manager** 

#### thinking highTEX

Sattler PRO-TEX GmbH Sattlerstraße 45, 8077 Gössendorf, Austria

Sitz Gössendorf, FN 425917z Landesgericht Graz UID-Nr.: ATU69256878

Tel +43 316 4104 0 Fax +43 316 4104 1351

mail@sattler.com protex.sattler.com Erste Bank AG, Wien IBAN: AT74 2011 1403 1318 6222, BIC: GIBAATWW

UniCredit Bank Austria AG, Graz





Reg.Nr.: 4048/6 Reg.Nr.: 405/6

1





CALIFORNIA DEPARTMENT OF FORESTRY and FIRE PROTECTION OFFICE OF THE STATE FIRE MARSHAL

## REGISTERED FLAME RESISTANT PRODUCT

Product:

787 POLYPLAN TENT OPAQUE

Registration No. F-06001

Product Marketed By: SATTLER AG SATTLERSTRASSE 45, 8077 GOSSENDORF AUSTRIA

This product meets the minimum requirements of flame resistance established by the California State Fire Marshal for products identified in Section 13115, California Health and Safety Code.

The scope of the approved use of this product is provided in the current edition of the CALIFORNIA APPROVED LIST OF FLAME RETARDANT CHEMICALS AND FABRICS, GENERAL AND LIMITED APPLICATIONS CONCERNS published by the California State Fire Marshal.

Deputy State Fire Marshal

Expire: 6/30/2021

FR-8

## DIVERSIFIED



TESTING LABORATORIES, INC. WORLDWIDE SERVICE

336 WEST FRONT STREET P.O. BOX 4004 BURLINGTON, NORTH CAROLINA 27215 PHONE (336) 227-7710 • FAX (336) 227-1175 www.diversifiedtestinglabs.com

December 19, 2013

Mr. Joe Santaloci OUTDURA CORP. 447 Main Street Hudson, NC 28638

Reference: Flammability Test Report Lab Identification No. 8543 Invoice No. 39305 (Attached)

Dear Mr. Santaloci:

One (1) fabric sample, identified as **787 POLYPLAN TENT OPAQUE**, was received and tested in accordance with the National Fire Prevention Association No. 701, "Standard Methods of Fire Tests for Flame Propagation of Textiles and Films, 2010 Edition, (Test 1, Small Scale)". The results are as follows:

Specimen Number	Residual Flame ( <u>seconds</u> )	Weight Loss ( <u>percent</u> )
1	0.0	4.41
2	0.0	3.80
3	0.0	3.81
4	0.0	2.33
5	0.0	3.97
6	0.0	2.96
7	0.0	3.96
8	0.0	3.95
9	0.0	4.18
10	0.0	4.15
AVG.	0.0	3.76

The fabric sample submitted **meets** the minimum requirements of the above standard. The average percent weight loss cannot exceed 40% and the weight loss of individual specimens cannot exceed mean value plus three standard deviations. The average residual flame cannot exceed 2.0 seconds.

If there are any questions or when we can be of further assistance, please let us know.

Sincerely,

Bobby E. Puett

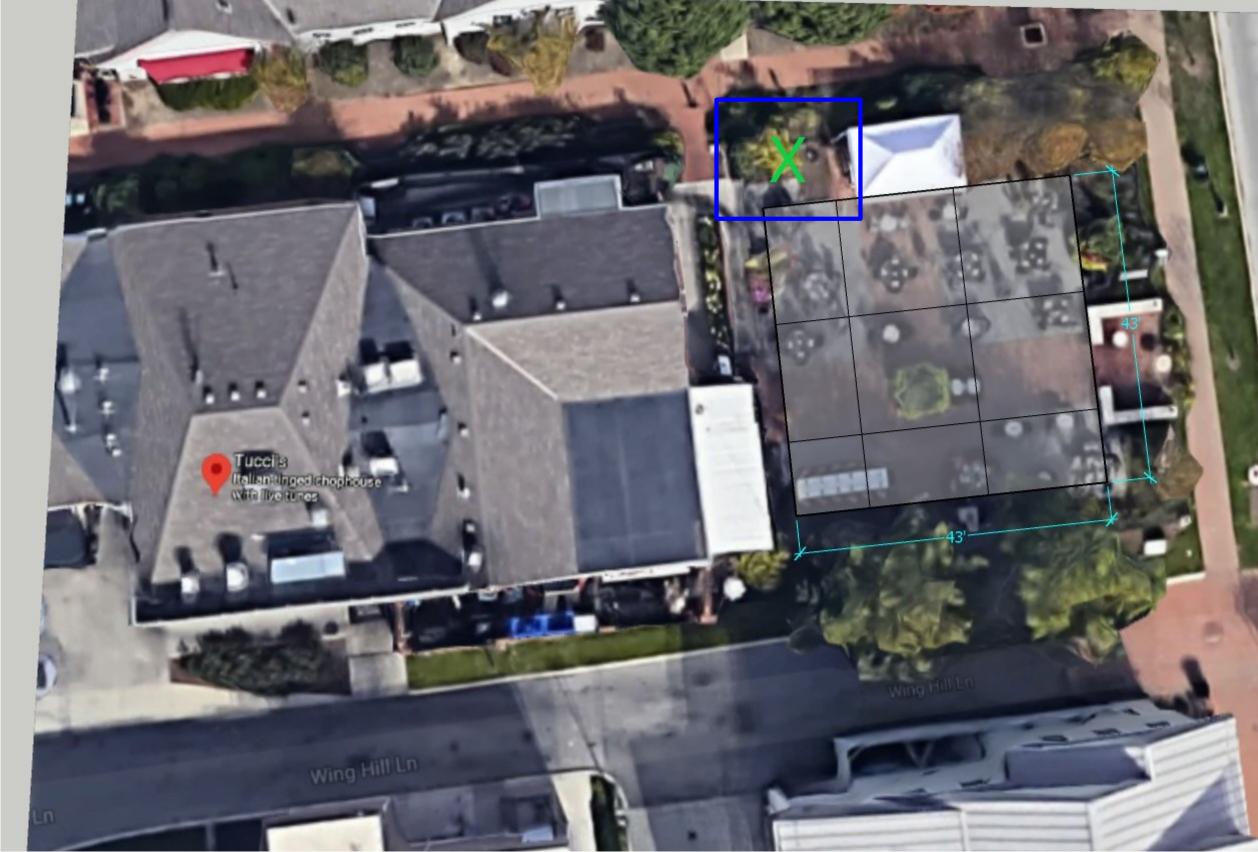
BEP/mr Attachment

OUR LETTERS AND REPORTS ARE FOR THE EXCLUSIVE USE OF THE CLIENT TO WHOM THEY ARE ADDRESSED. ANY COMMUNICATION TO OTHERS OR THE USE OF OUR COMPANY NAME MUST RECEIVE PRIOR APPROVAL. OUR TEST RESULTS APPLY ONLY TO THE SAMPLE TESTED AND ARE NOT NECESSARILY INDICATIVE OF THE QUALITIES OF APPARENTLY IDENTICAL OR SIMILAR PRODUCTS. SAMPLES NOT DESTROYED IN TESTING ARE RETAINED A MAXIMUM OF THIRTY DAYS. THE LETTERS, REPORTS OR NAME OF DIVERSIFIED TESTING LABORATORIES, INC. MAY NOT BE USED IN ADVERTISING TO THE GENERAL PUBLIC.

- "We Test Per Your Requise"

City of **ublin** 

OHIO, USA





City of D<u>ublim</u> ohio, usa roved for

## Screen HVAC per City Code.

 X = Temporary HVAC unit placed in existing landscaped area